

A Script of the Lecture

Theoretical Physics I
(Mechanics)

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1. Mathematical background

Given 2 Vectors \vec{A}, \vec{B} :

$$\vec{A} \cdot \vec{B} = A \cdot B \cos \theta$$

θ = angle between \vec{A}, \vec{B}

$$\vec{A} \times \vec{B} = \vec{C} \perp \vec{A}, \vec{B}$$

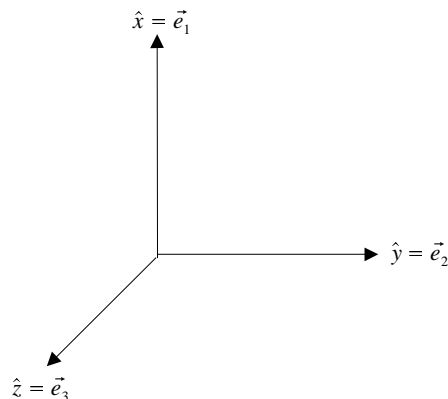
$$|\vec{C}| = A B \sin \theta$$

Vector: components in coordinates

reference frame: cartesian frame

$$\vec{x} = (x_1, x_2, x_3) = x_1 \vec{e}_1 + x_2 \vec{e}_2 + x_3 \vec{e}_3$$

\vec{e}_i are unit vectors along cartesian axes



Summation convention:

$$\vec{x} = x_i \vec{e}_i \hat{=} \sum_{i=1}^3 x_i \vec{e}_i$$

Metric of the space:

$$d = \sqrt{\sum_i (x_i - y_i)^2} \quad \text{Euclidean metric}$$

$$\vec{A} = (a_i), \vec{B} = (b_i)$$

$$\vec{A} \cdot \vec{B} = a_i b_i$$

$$\vec{A} \times \vec{B} = 0 \Leftrightarrow \vec{A} \uparrow \uparrow \vec{B} \text{ or } \vec{A} \uparrow \downarrow \vec{B}$$

$$\vec{A} \times \vec{B} = \begin{vmatrix} \vec{e}_1 & \vec{e}_2 & \vec{e}_3 \\ a_1 & a_2 & a_3 \\ b_1 & b_2 & b_3 \end{vmatrix} = \vec{e}_1 (a_2 b_3 - a_3 b_2) - \vec{e}_2 (a_1 b_3 - a_3 b_1) + \vec{e}_3 (a_1 b_2 - a_2 b_1)$$

$$\vec{A} \times (\vec{B} \times \vec{C}) = (\vec{A} \cdot \vec{C}) \vec{B} - (\vec{A} \cdot \vec{B}) \vec{C}$$

Position vector $\vec{x} = \vec{x}(t)$; $\vec{x}(t) = x_i(t) \vec{e}_i$

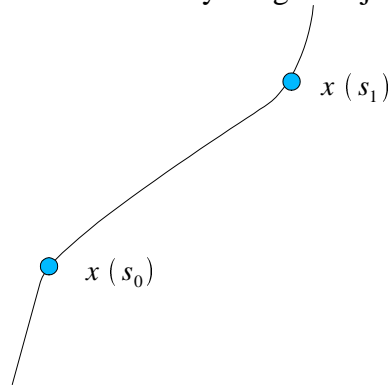
$$\frac{d(\vec{x}(t) \cdot \vec{y}(t))}{dt} = \frac{d\vec{x}}{dt} \cdot \vec{y} + \vec{x} \cdot \frac{d\vec{y}}{dt} = \dot{\vec{x}} \cdot \vec{y} + \vec{x} \cdot \dot{\vec{y}}$$

$$\int \vec{x}(t) dt = \vec{e}_i \int x_i(t) dt$$

1.0 Trajectories

$$\vec{x}(t), \vec{v}(t) = \dot{\vec{x}}(t)$$

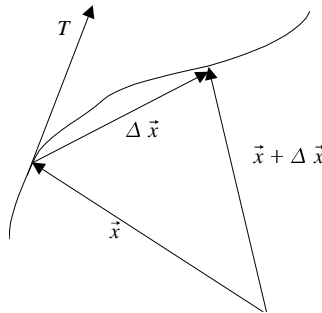
s parameter that increases smoothly and monotonically along the trajectory



$$\vec{x}(s_0) \text{ and } \vec{x}(s_1)$$

Distance along the trajectory:

$$l(s_0, s_1) = \int_{s_0}^{s_1} |\dot{\vec{x}}(s)| \, ds = \int_{s_0}^{s_1} \sqrt{\sum_i \dot{x}_i^2} \, ds$$



l as parameter

$$\vec{v} = \frac{d\vec{x}}{dt} = \frac{d\vec{x}}{dl} \frac{dl}{dt}$$

\vec{T} = tangent vector

$\Delta \vec{x}$ = coord vector

$$\vec{\tau} = \frac{d\vec{x}}{dl} = \lim_{l \rightarrow 0} \frac{\Delta \vec{x}}{\Delta l}$$

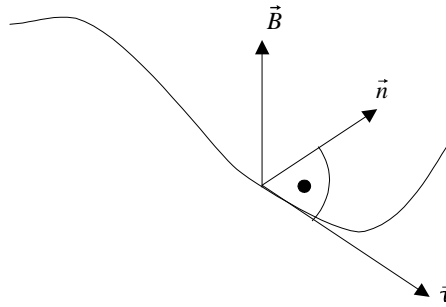
$|\Delta \vec{x}| = \Delta l \Rightarrow \vec{\tau}$ = unit vector tangent to the trajectory

$$\vec{v} = \vec{\tau} \frac{dl}{dt} = \vec{\tau} \cdot \dot{l} \text{ and } \vec{\tau} = \frac{d\vec{x}}{|d\vec{x}|} = \frac{\vec{v}}{|\vec{v}|}$$

\vec{v} is everywhere tangent to the trajectory and equal in magnitude to the speed \dot{l} along the trajectory.

Moving reference frames:

Osculating plane (Schmiegungeebene)

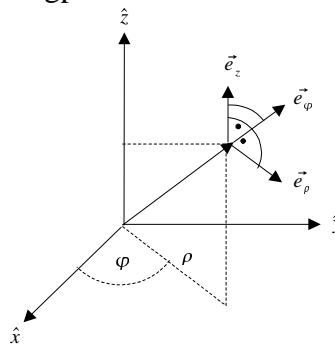


$$\vec{n} \perp \vec{\tau}, \quad \vec{n} = \frac{\dot{\vec{\tau}}}{|\dot{\vec{\tau}}|}$$

(**principal normal vector** –Hauptnormalenvektor)

$$\vec{\tau} \cdot \vec{\tau} = 1, \quad \frac{d}{dt} (\vec{\tau} \cdot \vec{\tau}) = 0 = 2 \vec{\tau} \frac{d}{dt} \vec{\tau}$$

The unit vector \vec{B} normal to the osculating plane is called **binormal vector** . (Binormalenvektor)



1.1 Coordinates systems

Cylindrical polar coordinates

- ρ radial distance from z
- ϕ angular rotation from x-axis
- z elevation above x-y-plane

Transformations

$$\vec{x} = (x, y, z) = (\rho \cos \phi, \rho \sin \phi, z)$$

$$\rho = \sqrt{x^2 + y^2}$$

$$\phi = \arctan \frac{y}{x}$$

Basis vectors : Point in the direction of increasing ρ , ϕ and z , respectively:

$$\vec{e}_\rho = \frac{\partial \vec{x} / \partial \rho}{|\partial \vec{x} / \partial \rho|} = \frac{(\cos \phi, \sin \phi, 0)}{1}$$

$$\vec{e}_\phi = \frac{\partial \vec{x} / \partial \phi}{|\partial \vec{x} / \partial \phi|} = \frac{(-\rho \sin \phi, \rho \cos \phi, 0)}{\rho} = (-\sin \phi, \cos \phi, 0)$$

$$\vec{e}_z = \frac{(\partial \vec{x} / \partial z)}{|\partial \vec{x} / \partial z|} = \frac{(0, 0, 1)}{1}$$

$$\Rightarrow \vec{x} = \rho \vec{e}_\rho + z \vec{e}_z$$

Velocity:

$$\begin{aligned} \dot{\vec{x}} &= \dot{\rho} \vec{e}_\rho + \rho \dot{\vec{e}}_\rho + \dot{z} \vec{e}_z + (z \dot{\vec{e}}_z) \\ \frac{d \vec{e}_\rho}{d t} &= \frac{\partial \vec{e}_\rho}{\partial \rho} \frac{d \rho}{d t} + \frac{\partial \vec{e}_\rho}{\partial \varphi} \frac{d \varphi}{d t} + \frac{\partial \vec{e}_\rho}{\partial z} \frac{d z}{d t} = 0 \\ \vec{e}_\rho &= (\cos \varphi, \sin \varphi, 0) \\ \frac{\partial \vec{e}_\rho}{\partial \varphi} &= (-\sin \varphi, \cos \varphi, 0) \\ \frac{d \vec{e}_\rho}{d t} &= (-\sin \varphi, \cos \varphi, 0) \cdot \dot{\varphi} = \dot{\varphi} \vec{e}_\varphi \\ \frac{d \vec{e}_\varphi}{d t} &= -\dot{\varphi} \vec{e}_\rho \\ \frac{d \vec{e}_z}{d t} &= 0 \\ \Rightarrow \dot{\vec{x}} &= \dot{\rho} \vec{e}_\rho + \rho \dot{\varphi} \vec{e}_\varphi + \dot{z} \vec{e}_z \\ \ddot{\vec{x}} &= (\ddot{\rho} - \rho \dot{\varphi}^2) \vec{e}_\rho + (\rho \ddot{\varphi} + 2 \dot{\rho} \dot{\varphi}) \vec{e}_\varphi + \ddot{z} \vec{e}_z \end{aligned}$$

1.2 Vectorcalculus

We define the **del operator**

$$\vec{\nabla} = \frac{\partial}{\partial x_1} \vec{e}_1 + \frac{\partial}{\partial x_2} \vec{e}_2 + \frac{\partial}{\partial x_3} \vec{e}_3$$

Scalar field (such as temperature)

$$\Phi(x_1, x_2, x_3)$$

The **gradient** of Φ is a vector field

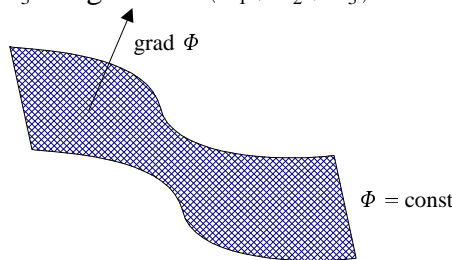
$$\vec{\nabla} \Phi = \frac{\partial \Phi}{\partial x_i} \vec{e}_i$$

$\vec{\nabla} \Phi$ lies perpendicular to surfaces of constant value $\Phi(x_1, x_2, x_3) = \text{const}$ which are termed **equipotential surfaces**.

For an arbitrary change in position, $d \vec{x} = (d x_1, d x_2, d x_3)$, the total derivative of Φ is given by

$$d \Phi = \vec{\nabla} \Phi \cdot d \vec{x} = \frac{\partial \Phi}{\partial x_i} d x_i = \left(\frac{\partial \Phi}{\partial x_1}, \frac{\partial \Phi}{\partial x_2}, \frac{\partial \Phi}{\partial x_3} \right) \cdot (d x_1, d x_2, d x_3).$$

We consider values of x_1, x_2, x_3 that give $\Phi(x_1, x_2, x_3) = \text{const}$.



$$d \Phi = 0 = \vec{\nabla} \Phi \cdot d \vec{x}, \text{ where } d \vec{x} \text{ lies within the equipotential surface.} \Rightarrow \Rightarrow \vec{\nabla} \Phi \perp d \vec{x}.$$

$$\vec{\nabla} \Phi \equiv \text{grad } \Phi$$

Calculate the gradient in terms of cylindrical polar coordinates:

$$\rho = \sqrt{x^2 + y^2}$$

$$\vec{e}_\rho = \cos \varphi \vec{e}_x + \sin \varphi \vec{e}_y$$

$$\varphi = \arctan \frac{y}{x}$$

$$\vec{e}_\varphi = -\sin \varphi \vec{e}_x + \cos \varphi \vec{e}_y$$

$$\text{grad } \Phi = \left(\frac{\partial \Phi}{\partial \rho} \frac{\partial \rho}{\partial x} + \frac{\partial \Phi}{\partial \varphi} \frac{\partial \varphi}{\partial x} + \frac{\partial \Phi}{\partial z} \frac{\partial z}{\partial x} \right) \vec{e}_x + \left(\frac{\partial \Phi}{\partial \rho} \frac{\partial \rho}{\partial y} + \frac{\partial \Phi}{\partial \varphi} \frac{\partial \varphi}{\partial y} + \frac{\partial \Phi}{\partial z} \frac{\partial z}{\partial y} \right) \vec{e}_y + \frac{\partial \Phi}{\partial z} \vec{e}_z$$

$$\frac{\partial \rho}{\partial x} = \frac{x}{\rho} = \cos \varphi$$

$$\frac{\partial \varphi}{\partial x} = \frac{1}{1 + \left(\frac{y}{x}\right)^2} \cdot \frac{-y}{x^2} = \frac{-\rho \sin \varphi}{\rho^2} = \frac{-\sin \varphi}{\rho}$$

$$\text{grad } \Phi = \frac{\partial \Phi}{\partial \rho} \vec{e}_\rho + \frac{\partial \Phi}{\partial \varphi} \frac{1}{\rho} \vec{e}_\varphi + \frac{\partial \Phi}{\partial z} \vec{e}_z$$

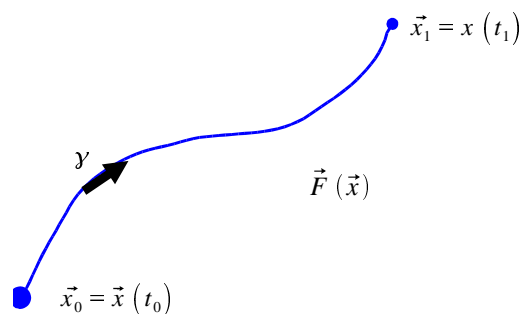
$$\text{grad } \Phi = \vec{e}_x \frac{\partial \Phi}{\partial x} + \vec{e}_y \frac{\partial \Phi}{\partial y} + \vec{e}_z \frac{\partial \Phi}{\partial z} = \frac{\partial \Phi}{\partial \rho} \vec{e}_\rho + \frac{\partial \Phi}{\partial \varphi} \frac{1}{\rho} \vec{e}_\varphi + \frac{\partial \Phi}{\partial z} \vec{e}_z;$$

$$\text{div } \vec{v} = \vec{\nabla} \cdot \vec{v} = \frac{\partial v_i}{\partial x_i} \equiv \sum_{i=1}^3 \frac{\partial v_i}{\partial x_i}$$

$$\vec{\nabla} = \vec{e}_x \frac{\partial}{\partial x} + \vec{e}_y \frac{\partial}{\partial y} + \vec{e}_z \frac{\partial}{\partial z};$$

$$\text{curl } \vec{v} = \vec{\nabla} \times \vec{v} = \begin{vmatrix} \vec{e}_1 & \vec{e}_2 & \vec{e}_3 \\ \frac{\partial}{\partial x_1} & \frac{\partial}{\partial x_2} & \frac{\partial}{\partial x_3} \\ v_1 & v_2 & v_3 \end{vmatrix} = \vec{e}_1 \left(\frac{\partial v_3}{\partial x_2} - \frac{\partial v_2}{\partial x_3} \right) - \vec{e}_2 \left(\frac{\partial v_3}{\partial x_1} - \frac{\partial v_1}{\partial x_3} \right) + \vec{e}_3 \left(\frac{\partial v_2}{\partial x_1} - \frac{\partial v_1}{\partial x_2} \right)$$

1.2.1 Lineintegrals



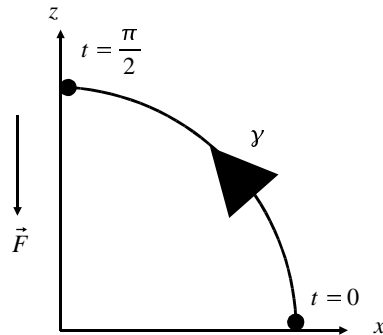
$$\int_{\gamma} \vec{F}(\vec{x}) \cdot d\vec{x} = \text{lineintegral of } \vec{F} \text{ along } \gamma$$

$$d\vec{x} = \frac{d\vec{x}}{dt} dt = \dot{\vec{x}} dt$$

$$\int \vec{F} \cdot d\vec{x} = \int_{t_0}^t F_x \dot{x} dt + \int_{t_0}^t F_y \dot{y} dt + \int_{t_0}^t F_z \dot{z} dt$$

$$F_z(\vec{x}(t)) \dot{z}(t)$$

Example:



$$\vec{F} = -g \vec{e}_z;$$

$$\vec{x}(t) = \begin{pmatrix} a \cos t \\ 0 \\ a \sin t \end{pmatrix}$$

$$\dot{\vec{x}}(t) = \begin{pmatrix} -a \sin t \\ 0 \\ a \cos t \end{pmatrix}$$

$$\vec{F} \cdot \dot{\vec{x}} = -g a \cos t$$

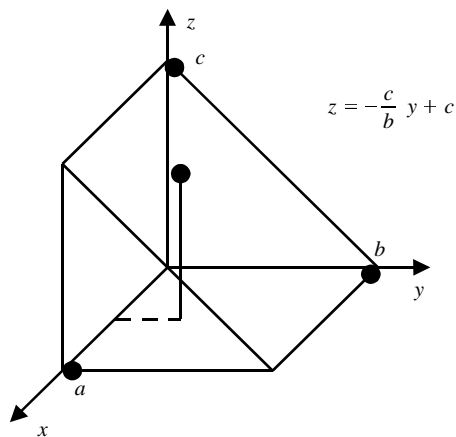
$$\int \vec{F} \cdot d\vec{x} = -g a \int_0^{\pi/2} \cos t dt = -g a$$

1.2.2 Multiple integrals

Body with mass density:

$$\mu = \lim_{\Delta V \rightarrow 0} \frac{\Delta M}{\Delta V} = \mu_0$$

Specifically, **wedge**: Calculate M :

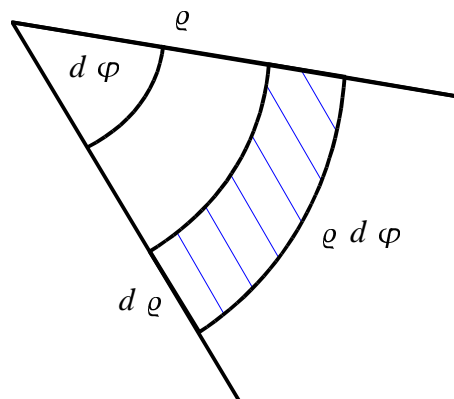
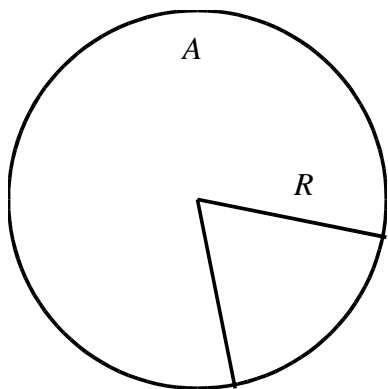


$$\begin{aligned}
 M &= \int \int \int_{\text{wedge}} \mu(x, y, z) \, dx \, dy \, dz = \mu_0 \int_0^a dx \int_0^b dy \int_0^{-\frac{c}{b}y+c} dz \cdot 1 \\
 &= \mu_0 \int_0^a dx \int_0^b dy \left(-\frac{c}{b}y + c \right) = \mu_0 \int_0^a dx \left(-\frac{c}{b} \frac{y^2}{2} + cy \right)_0^b \\
 &= \mu_0 \int_0^a dx \left(-\frac{cb}{2} + cb \right) = \mu_0 \frac{abc}{2};
 \end{aligned}$$

Consider circle of constant **areadensity** :

$$\sigma = \lim_{\Delta A \rightarrow 0} \frac{\Delta M}{\Delta A} = \sigma_0$$

Calculate M :



$$M = \int \int_{\text{circle}} \sigma \, dA$$

polar coord: ρ, φ ;

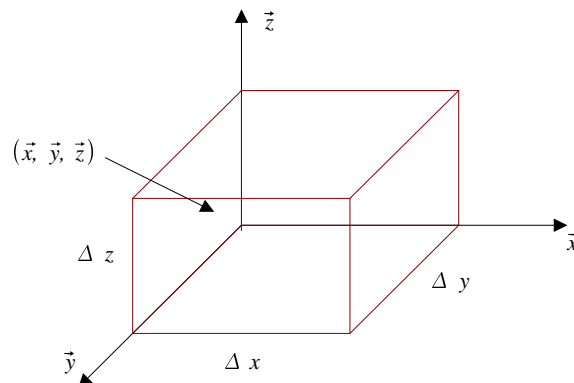
$$dA = dx \, dy = d\rho \cdot \rho \, d\varphi ;$$

$$M = \sigma_0 \int_{\rho=0}^R d\rho \rho \int_{\varphi=0}^{2\pi} d\varphi = \pi \sigma_0 R^2$$

3 D: $d\rho \rho \, d\varphi \, dz = dV$

1.3 Gauss's Theorem

Momentum field where $\vec{u} = \rho \vec{v}$ gives the momentum carried per unit volume (ρ is the mass density, \vec{v} velocity).



Mass that flows in and out of the box.

\vec{v} is constant across each surface plane of the box.

I_x = Rate of flow in at x = mass that flows in per unit time at $x = \rho v_x(x) \Delta y \Delta z$;

O_x = Rate of flow out at $x + \Delta x$ =

$$\rho v_x(x + \Delta x) \Delta y \Delta z = \rho \left(v_x(x) + \frac{\partial v_x}{\partial x} \Delta x \right) \Delta y \Delta z;$$

$$O_x - I_x = \rho \frac{\partial v_x}{\partial x} \Delta x \Delta y \Delta z = \text{Net outward flow.}$$

$O - I$ = net flow out of the box =

$$\rho \underbrace{\left(\frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial z} \right)}_{\vec{\nabla} \cdot \vec{v}} \Delta x \Delta y \Delta z;$$

Net flow = density \times component of velocity normal to the surface \times

$$\text{Area of surface} = \sum_{\text{surface of the box}} \rho \vec{n} \cdot \vec{v} \Delta S$$

Gauss's Theorem or Divergence Theorem

$$\iiint_V \vec{\nabla} \cdot \vec{A} \, dV = \iint_S \vec{n} \cdot \vec{A} \, dS$$

\vec{A} : any vector field;

S : surface that bounds V ;

\vec{n} = unit vector normal to S , pointing outward

1.4 Stokes's Theorem

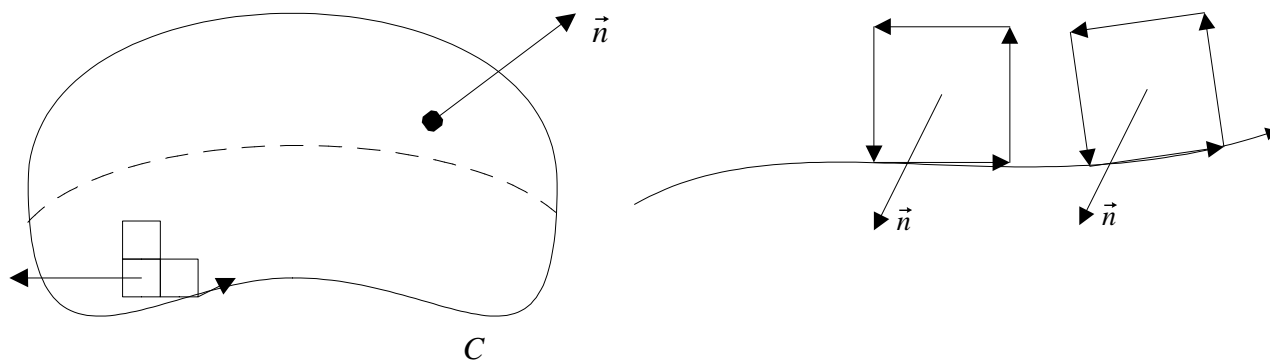
Surface integral over the curl of a vector field = line integral of that vector field along the boundary

of the surface.

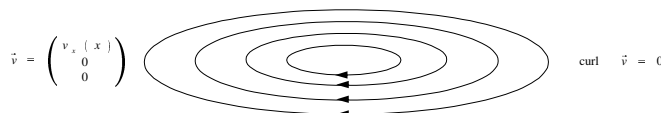
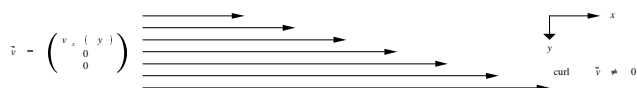
$$\int_S (\vec{\nabla} \times \vec{v}) \cdot \vec{n} \, dS = \oint_C \vec{v} \cdot d\vec{r}$$

$C = \partial S = \text{boundary of } S$

\vec{n} is the unit vector to the surface element dS , pointing outwards



The direction used in evaluating the line integral is given by the right hand rule with respect to \vec{n} .



1.5 Ordinary differential equations

1.5.1 Basic definitions

An ODE of order n has the form

$$y^{(n)}(x) = f(x, y(x), y'(x), \dots, y^{(n-1)}(x)).$$

Theorem 1: Its general solution has the form

$$y = y(x; c_1, \dots, c_n)$$

where c_1, \dots, c_n are arbitrary real constants. For a complete and unique specification of the solution, n initial values must be specified.

$$y(x_0) = y_0, y'(x_0) = y_0^{(1)}, y''(x_0) = y_0^{(2)}, \dots, y^{(n-1)}(x_0) = y_0^{(n-1)}$$

Initial Value Problem (IVP)

Theorem 2: Every ODE of n -th order can be transformed into a set of n first-order ODEs.

$$1) \quad y^{(n)}(x) = f(x, y'(x), \dots, y^{(n-1)}(x))$$

$$2) \text{ Introduce new variables: } y_1 = y, \quad y_2 = y', \dots, \quad y_n = y^{(n-1)}$$

3) System of 1st order ODEs:

$$y'_1 = y_2, \quad y'_2 = y_3, \dots, \quad y'_{n-1} = y_n, \quad y'_n = f(x, y_1, y_2, \dots, y_n).$$

Note: A partial differential equation $F(x_1, \dots, x_n, u, u_{x_1}, \dots, u_{x_n}, u_{x_1 x_1}, \dots, u_{x_n x_n}) = 0$

1.5.2 Special cases

Type 1: ODE that allows **separation of variables**

$$\frac{dy}{dx} = y' = \frac{f(x)}{g(y)} \Rightarrow \int g(y) dy = \int f(x) dx + C \text{ is general solution}$$

Type 2: Linear first-order ODE

$$y' + f(x)y = g(x)$$

with

$$M(x) = e^{\int f(x) dx},$$

the general solution is

$$y(x) = \frac{1}{M(x)} \left[\int g(x) M(x) dx + C \right]$$

Example: $y' + \frac{1}{x}y = x^2$

$$M(x) = e^{\int \frac{1}{x} dx} = e^{\ln x} = x$$

$$y(x) = \frac{1}{x} \left[\int x^3 dx + C \right] = \frac{x^3}{4} + \frac{C}{x};$$

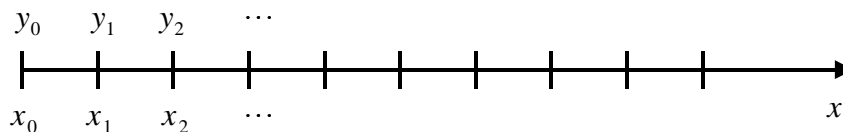
1.5.3 Numerical solution for ODEs

IVP: $y' = f(x, y); \quad y(x_0) = y_0; \Rightarrow y(x) = ?$

By discretization: $h > 0$

convert x -space \rightarrow coarse-grained space

$$x_0, x_0 + h = x_1, x_1 + h = x_2, \dots$$



This so-called, **forward Euler method** “takes solution at $x_n \rightarrow x_{n+1}$:

$$y_{n+1} = y_n + h \cdot f(x_n, y_n)$$

Start: $n = 0 \dots (x_n, y_n) = y(x)|_n$

2.PrinciplesofDynamics

- Motionofobjectsacteduponbyexternalforces.
- Pointparticles,characterizedby $\vec{x} = \vec{x}(t)$ with $\vec{v}(t) = \dot{\vec{x}}(t)$
- t „time“–before–after,assumethat
 $(\vec{x}_i(t), \vec{v}_i(t))_{i=1, \dots, N}$
 canbemeasured *simultaneously*
 Assumption: $|\vec{v}_i| \ll c$
- Assumethat \vec{x} and \vec{v} canbemeasuredforeachpointparticle: \Rightarrow outofquantummechanics

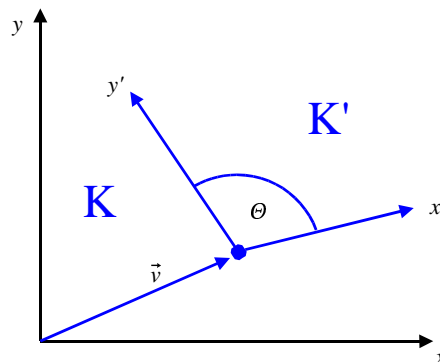
2.1Newton'slaws

Physicalsepace:3 D, Euclideanmetric

Principle 1 (Newton's first law): There exist certain frames of reference, called **inertial**, with prop's:
 A. Every isolated particle moves in a straight line in such a frame.
 B. Every isolated particle moves at constant velocity in this frame.

Consequences

- Theexistenceofoneinertialframeimpliestheexistenceofmanymore.
- DuetetoA, theycannotrotatewithrespecttoeachother.



- Transformations: **Galileian**

Principle2(3rdNewton'slaw) :

A. ConservationofMomentum :

Consider 2 particles, isolated from all other matter, from an inertial frame, with velocities $\vec{v}_j(t)$, $j = 1, 2, \dots$.

Then there exists a constant $\mu_{12} > 0$ and a constant vector \vec{K} independent of time suchthat

$$\vec{v}_1(t) + \mu_{12} \vec{v}_2(t) = \vec{K}.$$

μ_{12} isuniversal(i.e.neitherdependsoninertialframenoronparticularmotion).

B. ExistenceofMass :

Bringinathirdparticlesuchthatwatch1-3andthen2-3.

$$\begin{aligned}\vec{v}_3(t) + \mu_{31} \vec{v}_1(t) &= \vec{M} \\ \vec{v}_2(t) + \mu_{23} \vec{v}_3(t) &= \vec{L} \\ \text{Then:} \\ \mu_{12} \mu_{23} \mu_{31} &= 1 \quad (3)\end{aligned}$$

(3) $\Rightarrow \exists m_i > 0$ ($i = 1, 2, 3$) such that (1) + (2):

$$m_1 \vec{v}_1(t) + m_2 \vec{v}_2(t) = \vec{P}_{12}$$

$$m_2 \vec{v}_2(t) + m_3 \vec{v}_3(t) = \vec{P}_{23}$$

$$m_3 \vec{v}_3(t) + m_1 \vec{v}_1(t) = \vec{P}_{31}$$

\vec{P}_{ij} , called **momenta** (Impulse), is constant.

– Masses are *not* unique, only ratios μ of masses is unique. Standard must be chosen (e.g. 1 cm³ of water at 4 °C and atmospheric pressure).

– $\frac{d}{dt}$ (4)

$$\Rightarrow m_i \vec{a}_i + m_j \vec{a}_j = 0 \quad (i \neq j)$$

Define the force acting on a particle by

$$\vec{F} = m \vec{a} = m \frac{d^2 \vec{x}}{dt^2}.$$

Newton's second law: Particles 1 and 2: \vec{a}_1 of particle 1 arises as a result of the interaction between 1-2. One says there is a **force** $\vec{F}_{12} = m_1 \vec{a}_1$ on particle 1 due to the presence of particle 2 or by particle 2. Also, $\vec{F}_{21} = m_2 \vec{a}_2$ on particle 2 by particle 1.

$$\vec{F}_{12} + \vec{F}_{21} = 0.$$

To every **action** there is an equal and opposite **reaction**.

Newton's 3rd law:

$$\vec{F} = m \frac{d^2 \vec{x}}{dt^2}.$$

Forces satisfy the **superposition principle**. The total force on a particle can be found by adding contributions from different agents.

Remark: For gravitation, \vec{a} is known a priori.

2.2 Stability of solutions

\vec{F} is given $\vec{x}, \dot{\vec{x}}, t$

Set of 3rd-order ODEs

$$\vec{F}(\vec{x}, \dot{\vec{x}}, t) = m \ddot{\vec{x}}$$

$$\vec{x}(t_0), \dot{\vec{x}}(t_0)$$

Stability of solutions

$$\vec{x}_1(t_0) \text{ and } \vec{x}_2(t_0) = \vec{x}_1(t_0) + \delta \vec{x}(t_0)$$

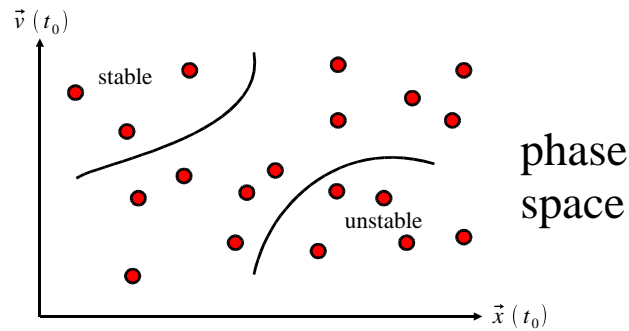
$$D \vec{x}(t) = |\delta \vec{x}(t_0)| < \varepsilon \text{ and assume } \dot{\vec{x}}_1(t_0) = \dot{\vec{x}}_2(t_0)$$

Then solutions are **stable** if

$$\lim_{t \rightarrow \infty} D \vec{x}(t) = O(D \vec{x}(t_0))$$

and **unstable** if

$$\lim_{t \rightarrow \infty} D \vec{x}(t) = \infty$$



Regions, stable + unstable solutions are mixed together tightly. Such a system is called **chaotic** (in given portion of phase space), **exhibits chaos**.

2.3 One-particle dynamical variables

$$\vec{F} = m \vec{a} \Rightarrow \vec{x}(t)$$

Symmetry $\Rightarrow f(\vec{x}, \dot{\vec{x}}, t)$

dynamical variables characterize motion

2.3.1 Momentum

$$\vec{p} = m \vec{v} \Rightarrow \vec{F} = \frac{d}{dt} \vec{p}$$

$$\vec{F} = 0 \Rightarrow \vec{p} = \text{conserved}$$

If total force = 0, \vec{p} is a constant of motion.

$$\text{Note: } m = m(t), \vec{v} = \vec{v}(t) \Rightarrow \vec{p}$$

Assumption: All measurements are performed in inertial systems.

2.3.2 Angular momentum

\vec{L} about some point \vec{S} :

$$\vec{L} = \vec{x} \times \vec{p}$$

where \vec{x} is measured from the point \vec{S} .

\vec{S} must be **inertial point**, moves at $\vec{v} = \text{const}$ in any inertial frame.

$$\dot{\vec{L}} = \frac{d}{dt} (\vec{x} \times \vec{p}) = \underbrace{\dot{\vec{v}} \times \vec{p}}_{=0} + \vec{x} \times \underbrace{\dot{\vec{p}}}_{=\vec{F}};$$

$$\dot{\vec{L}} = \vec{x} \times \vec{F} = \vec{N}$$

torque(Drehmoment) about \vec{S}

$$\dot{\vec{p}} = \vec{F}$$

$$\vec{N} = 0 \Rightarrow \vec{L} = \text{const}$$

2.3.3 Energy and work

Often, $\vec{F}(\vec{x})$

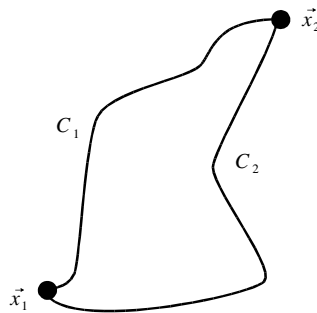
$$\int_{C: \vec{x}(t_0)}^{\vec{x}(t)} \vec{F}(\vec{x}) \cdot d\vec{x} = \int_{t_0}^t \vec{F}(\vec{x}) \cdot \dot{\vec{x}} dt = m \int_{t_0}^t \ddot{\vec{x}} \cdot \dot{\vec{x}} dt = \frac{1}{2} m \int_{t_0}^t \frac{d}{dt} (\dot{\vec{x}}^2) dt = \frac{1}{2} m v^2(t) - \frac{1}{2} m v^2(t_0);$$

T kinetic energy

Kinetic energy $T = 1/2 m v^2$ and the work W_C done by the force along C :

$$W_C = \int_C \vec{F} \cdot d\vec{x}.$$

If W is not path-dependent, the force is called **conservative force**:



Conservative: \Rightarrow

$$\int_{C_1} \vec{F} \cdot d\vec{x} = \int_{C_2} \vec{F} \cdot d\vec{x};$$

$$\int_{C_1} \vec{F} \cdot d\vec{x} - \int_{C_2} \vec{F} \cdot d\vec{x} = \oint \vec{F} \cdot d\vec{x} = 0.$$

If \vec{F} conservative,

$$\oint \vec{F} \cdot d\vec{x} = 0$$

around *any* closed path, for \vec{x}_1, \vec{x}_2 arbitrary.

$$\oint_{C = \partial \Sigma} \vec{F} \cdot d\vec{x} = \int_{\Sigma} (\vec{\nabla} \times \vec{F}) \cdot d\vec{S}$$

Σ is a smooth surface bounded by the closed path $C = \partial \Sigma$.

$$\vec{\nabla} \times \vec{F} = 0 \Leftrightarrow F = \text{conservative}$$

curl grad $V \equiv 0$;

$$\vec{\nabla} \times (\vec{\nabla} V) \equiv 0 ;$$

$$\vec{F}(\vec{x}) = -\vec{\nabla} V(\vec{x}) ;$$

$V(\vec{x})$ potential energy

Note: \vec{V} is not unique and defined only up to an additive constant.

$$W_C = W(\vec{x}, \vec{x}_0) = \int_{\vec{x}_0}^{\vec{x}} \vec{F}(\vec{x}') \cdot d\vec{x}' = - \int_{\vec{x}_0}^{\vec{x}} \vec{\nabla} V(\vec{x}') \cdot d\vec{x}' = V(\vec{x}_0) - V(\vec{x}) \equiv V_0 - V$$

$$V_0 - V = T - T_0 ; V + T = V_0 + T_0 = E = \text{const} ;$$

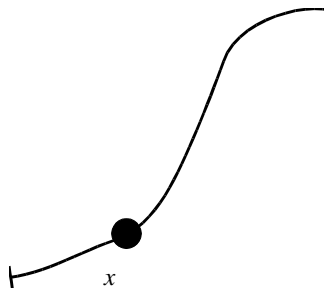
E total mechanical energy

\Rightarrow conservation of energy for conservative forces

Note: E is also defined only up to an additive constant; usual: $V(\vec{x}_0) = 0$.

2.3.4 Application to 1-D motion

Number of functions of time needed to describe fully the system is called **number of degrees of freedom** or **number of freedoms**.



\Rightarrow one-freedom system, can be reduced to **quadrature**

x : distance along line

F along line $= F(x) \Rightarrow$ necessarily conservative

$$\Rightarrow m \ddot{x} = - \frac{dV(x)}{dx} .$$

The energy

$$\frac{1}{2} m \dot{x}^2 + V(x) = E \quad (*)$$

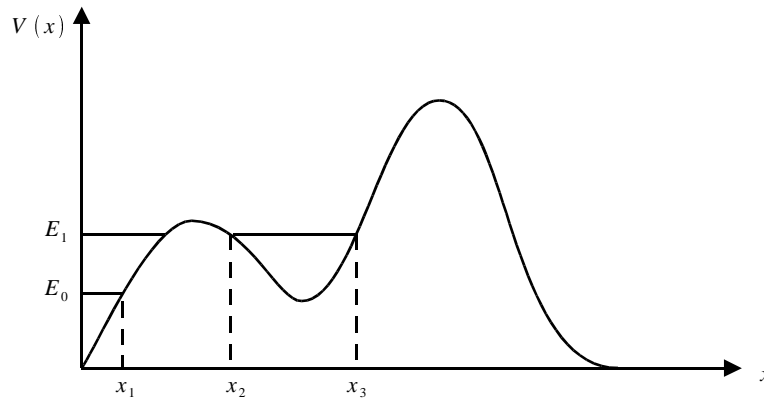
$\frac{1}{2} m \dot{x}^2 + V$ energy first-integral

$$\frac{1}{\dot{x}} = \frac{d t}{d x} \Rightarrow (*) \Rightarrow$$

$$t - t_0 = \sqrt{\frac{m}{2}} \int_{x_0}^x \frac{d x}{\sqrt{E - V(x)}}$$

$$x_0 = x(t_0), x = x(t)$$

$$\Rightarrow x = x(t - t_0, E)$$



$$\underbrace{\frac{1}{2} m \dot{x}^2}_{> 0} + V(x) = E$$

Particle cannot enter region $E = V(x) < 0$

– $E - V(x) > 0 : E = E_0$

If particle moves:

$$V \uparrow \Rightarrow \frac{1}{2} m \dot{x}^2 \downarrow$$

until $E - V(x) = 0 : \dot{x} = 0 \Rightarrow x_1$.

$$\text{At } x_1 : F(x_1) = - \left. \frac{d V}{d x} \right|_{x_1} < 0$$

\Rightarrow particle gets accelerated to the left

– $E_1 : x_2 < x < x_3$ motion *bounded*

Period:

$$P = \sqrt{2 m} \int_{x_2}^{x_3} \frac{d x}{\sqrt{E - V(x)}}$$

– $\frac{d V}{d x} = 0$ **equilibration points**

can be *stable* (minima) or *unstable* (maxima)

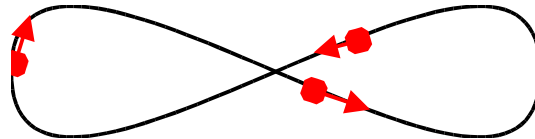
2.4 Many-particlesystem

2.4.1 Superposition principle

$N > 1$ particles may interact with one another and also are acted on by external forces.

Only 2-particle problem can be solved generally and analytically.

A. Chenciner and R. Montgomery: 3 particles, equal mass, interact via gravitation; discovered the first exact, stable and periodic nontrivial solution of 3-body-problem



Superposition principle: Total force acting on a particle is a vector sum of all the forces exerted on it by each of the other particles in the system (the **internal forces**) plus all of the **external forces**.

Superposition principle implies that all forces can be analyzed in terms of *2-particle interactions*.

A, B, C . The force on A is the sum of the force it would feel if only B were present and the force it would feel if only C were present.

This superpositional principle is an additional assumption to Newton's laws, it is a result of experimental observation.

⇒ Assume two-body forces

2.4.2 Center of Mass

\vec{F}_{ij} = force exerted on i -th particle by the j -th particle. ⇒ $\vec{F}_{ii} = 0$

Newton's 3rd law ⇒ $\vec{F}_{ij} = -\vec{F}_{ji}$

Note: Abandon the summation convention in this section!

$$m_i \ddot{\vec{x}}_i = \vec{F}_i + \sum_{j=1}^N \vec{F}_{ij}$$

$$\sum_i m_i \ddot{\vec{x}}_i = \underbrace{\sum_i \vec{F}_i}_{=\vec{F}} + \underbrace{\sum_{i,j} \vec{F}_{ij}}_{=0}$$

\vec{F} total external force = sum over only external forces

$$M = \sum_i m_i \Rightarrow$$

$$\vec{F} = M \left(\frac{1}{M} \sum_i m_i \ddot{\vec{x}}_i \right) \equiv M \ddot{\vec{X}};$$

$$\vec{X} \equiv \frac{1}{M} \sum_{i=1}^N m_i \vec{x}_i \quad \text{center of mass}$$

Center-of-mass theorem: The center of mass of N -particle system moves as though the total mass were concentrated there and were acted upon by the total external force.

2.4.3 Momentum

Total momentum

$$\vec{p} = \sum_i m_i \dot{\vec{x}}_i = M \dot{\vec{X}}$$

$$\Rightarrow \vec{F} = \dot{\vec{P}}$$

if $F_{ext} = 0 \Rightarrow \vec{P} = \text{const}$

$$\Rightarrow M \text{ constant} \Rightarrow \dot{\vec{X}} = \text{const} \Rightarrow \vec{X} = \vec{x}_0 + \underbrace{\vec{C}}_{=\frac{\vec{P}_0}{m}} t$$

\Rightarrow 6 conserved dynamical variables associated with center of mass

2.4.4 Energy

$\vec{y}_i = \vec{x}_i - \vec{X}$ position of the i -th particle *relativeto the center of mass*

$$T = \frac{1}{2} \sum_i m_i \dot{\vec{x}}_i^2 = \frac{1}{2} M \dot{\vec{X}}^2 + \frac{1}{2} \sum_i m_i \dot{\vec{y}}_i^2$$

Total work done on all particles: initial configuration $\{0\}$ (3 N coordinates) \rightarrow final configuration $\{f\}$ (3 N momenta)

$$\sum_i \int_{\vec{x}_{i0}}^{\vec{x}_{if}} \left(\vec{F}_i + \sum_j \vec{F}_{ij} \right) \cdot d\vec{x}_i = \underbrace{\sum_i \int_{\vec{x}_{i0}}^{\vec{x}_{if}} m_i \ddot{\vec{x}}_i \cdot d\vec{x}}_{T_f - T_i}$$

r.h.s.: $T_f - T_0$

Assume: $\vec{F}_i = -\vec{\nabla}_i V_i(\vec{x}_i)$; $\vec{F}_{ij} = -\vec{\nabla}_i V_{ij}(|\vec{x}_i - \vec{x}_j|)$.

$$\Rightarrow \vec{F}_{ji} = -\vec{F}_{ij}$$

$$\sum_i \int_{\vec{x}_{i0}}^{\vec{x}_{if}} \vec{F}_i \cdot d\vec{x}_i = \sum_i (V_i^0 - V_i^f) = V_{ext}^0 - V_{ext}^f;$$

$$\int_{\vec{x}_{i0}}^{\vec{x}_{if}} \sum_j \vec{F}_{ij} \cdot d\vec{x}_i = \frac{1}{2} \left(\sum_{ij} \vec{F}_{ij} \cdot d\vec{x}_i + \sum_{ij} \underbrace{\vec{F}_{ji}}_{=-\vec{F}_{ij}} \cdot d\vec{x}_j \right) = \frac{1}{2} \int_{\vec{x}_{i0}}^{\vec{x}_{if}} \sum_{ij} \vec{F}_{ij} \cdot d \underbrace{(\vec{x}_i - \vec{x}_j)}_{\vec{x}_{ij}}$$

$$= \frac{1}{2} \int_{\vec{x}_{i0}}^{\vec{x}_{if}} \sum_{ij} \vec{F}_{ij} \cdot d\vec{x}_{ij} = \frac{1}{2} \sum_{ij} (V_{ij}^0 - V_{ij}^f) = V_{int}^0 - V_{int}^f$$

$$\Rightarrow (V_{ext} + V_{int} + T)^0 = (V_{ext} + V_{int} + T)^f = E$$

Note: We have assumed that the internal forces can be derived from

$$V_{ij}(x), x = |\vec{x}_i - \vec{x}_j|$$

$$\Rightarrow \vec{F}_{ij} = -\frac{dV_{ij}(x)}{dx} \frac{\vec{x}_i - \vec{x}_j}{|\vec{x}_i - \vec{x}_j|}$$

Central force acting along the connecting line between \vec{x}_i and \vec{x}_j . This implies:

$$(\vec{x}_i - \vec{x}_j) \times \vec{F}_{ij} = 0;$$

This is a supplement to the 3rd Newton's principle.



2.4.5 Angular momentum

Inertial reference system: Compute the total angular momentum about the origin.

$$\vec{L} = \sum_i m_i \vec{x}_i \times \dot{\vec{x}}_i = \sum_i \vec{x}_i \times \vec{p}_i$$

The total angular momentum about the center of mass is

$$\vec{L}_c = \sum_i m_i \vec{y}_i \times \dot{\vec{y}}_i; \quad \vec{y}_i = \vec{x}_i - \vec{X}$$

$$\vec{L} = \sum_i m_i (\vec{X} + \vec{y}_i) \times (\dot{\vec{X}} + \dot{\vec{y}}_i) = \sum_i m_i \vec{X} \times \dot{\vec{X}} + \sum_i m_i \vec{y}_i \times \dot{\vec{y}}_i + \underbrace{\sum_i m_i \vec{y}_i \times \dot{\vec{X}}}_{=0} + \underbrace{\sum_i m_i \vec{X} \times \dot{\vec{y}}_i}_{=0}$$

(3rd sum: position of center of mass relative to itself; 4th sum: velocity of center of mass relative to itself)

$$\vec{L} = \vec{L}_c + M \vec{X} \times \dot{\vec{X}}$$

The total angular momentum about the origin of an inertial system = sum of the angular momenta of the total mass as though all the mass were concentrated at the center of mass + inertial angular momentum = angular momentum about the center of mass.

Question: Does $N = \dot{\vec{L}}$ hold also for many-particlesystem?

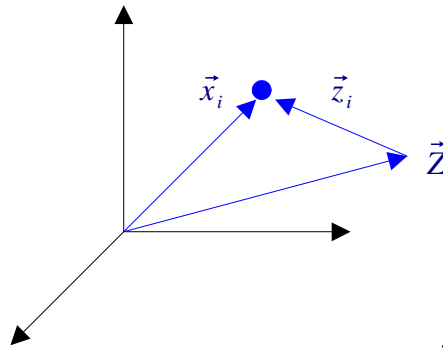
Supplement to 3rd Newton's law about \vec{F}_{ij} guarantees that the internal torques do not contribute to the change in the total angular momentum.

⇒ Need to consider solely the externally applied torque.

The external forces apply a total torque about an arbitrary (moving) point \vec{Z} :

$$\vec{N}_Z = \sum_i \vec{z}_i \times \vec{F}_i = \sum_i m_i \vec{z}_i \times \dot{\vec{x}}_i,$$

where \vec{x}_i = position of i -th particle in an inertial frame; $\vec{z}_i = \vec{x}_i - \vec{Z}$ is its position relative to \vec{Z} .



$$\vec{N}_Z = \sum_i m_i \vec{z}_i \times (\ddot{\vec{z}}_i + \ddot{\vec{Z}}) = \frac{d}{dt} \sum_i m_i \vec{z}_i \times \dot{\vec{z}}_i + M (\vec{X} - \vec{Z}) \times \ddot{\vec{Z}} = \vec{L}_Z + M (\vec{X} - \vec{Z}) \times \ddot{\vec{Z}};$$

$$\vec{N}_Z = \dot{\vec{L}}_Z \text{ if } \vec{X} - \vec{Z} \parallel \ddot{\vec{Z}}$$

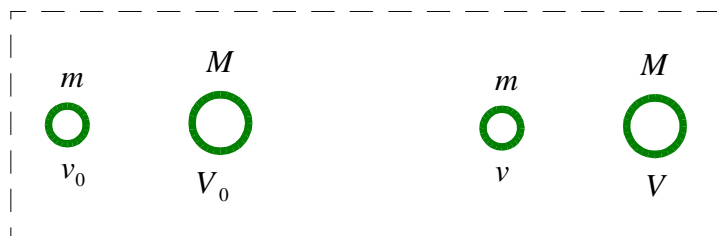
special cases are:

- $\ddot{\vec{Z}} = 0 \Rightarrow \vec{Z}$ is moving at constant velocity relative to the origin of the inertial frame
- $\vec{X} = \vec{Z} \Rightarrow \vec{Z}$ is chosen as the center of mass of the system.

[<http://www.ai.mit.edu/people/wessler/halo/mont.html>]

2.5 Examples

2.5.1 One-dimensional collision between point particles



Conservation of total momentum:

$$m v_0 + M V_0 = m v + M V$$

$$m (v - v_0) = M (V - V_0) (*)$$

$$x_{CM} = \frac{m x_0 + M X_0}{m + M}$$

$$\frac{m v_0 + M V_0}{m + M} = \frac{m v + M V}{m + M}$$

Elastic collision – energy conserved:

$$\frac{m v_0^2}{2} + \frac{M V_0^2}{2} = \frac{m v^2}{2} + \frac{M V^2}{2};$$

$$m (v^2 - v_0^2) = M (V^2 - V_0^2)$$

$$(*) \rightarrow v + v_0 = V_0 + V (**)$$

(*) & (**) \Rightarrow

$$V = \frac{M - m}{m + M} V_0 + \frac{2m}{m + M} v_0;$$

$$v = \frac{m - M}{m + M} v_0 + \frac{2M}{m + M} V_0;$$

Fully inelastic collision:

$$v = V$$

Conservation of momentum:

$$m v_0 + M V_0 = (m + M) v$$

$$v = \frac{m v_0 + M V_0}{m + M};$$

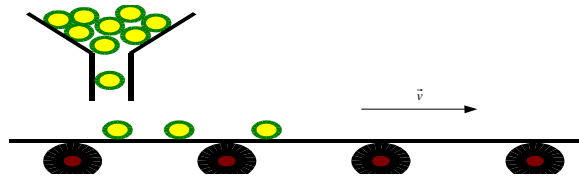
$$E_{kin, initial} = \frac{m}{2} v_0^2 + \frac{M}{2} V_0^2;$$

$$E_{kin, final} = \frac{m + M}{2} v^2 = \frac{1}{2} \frac{(m v_0 + M V_0)^2}{m + M};$$

$$\Delta E_{loss}^{kin} = E_{kin, initial} - E_{kin, final} = \frac{\mu}{2} (v_0 - V_0)^2;$$

$$\frac{1}{\mu} = \frac{1}{m} + \frac{1}{M};$$

2.5.2 Example: Conveyor belt



m : mass of the material (on the belt)

M : mass of the belt

v : velocity of the system

Force?

Which force is needed to keep a conveyor belt moving at constant speed of 5 m/s, if the material gets dumped onto the belt at constant rate $\frac{dm}{dt} = 100 \text{ kg/s}$?

The total momentum is

$$P = (m + M) v;$$

$$F = \frac{dP}{dt} = v \frac{dm}{dt} = 5 \cdot 100 \text{ N};$$

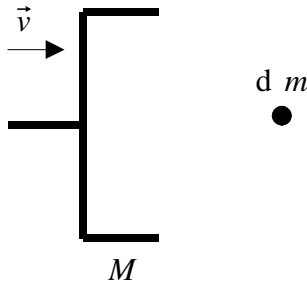
The power, i.e. the energy transfer per unit of time

$$\frac{dW}{dt} = \vec{F} \cdot \frac{d\vec{x}}{dt} = F v = v^2 \frac{dm}{dt} = \frac{d}{dt} (m v^2) = \frac{d}{dt} (m v^2 + M v^2) = \frac{d}{dt} ((m + M) v^2) = \frac{d}{dt} (2$$

;

2.5.3 Example: snowplow

(british: plough)



$$dE_{kin} = \frac{dm M}{2(M + dm)} (0 - v)^2 = \frac{1}{2} dm v^2$$

$$v_{dm} = v_M = \frac{M v}{M + dm} \approx v \left(1 - \frac{dm}{M} \right) + \dots$$

$$E_{initial} = \frac{1}{2} M v^2$$

$$E_{final} = \frac{1}{2} (M + dm) v^2$$

i.e.:

$$dE_{kin} = E_{kin, final} - E_{kin, initial} = \frac{1}{2} dm v^2$$

$$\frac{dE}{dt} = 2 \cdot \frac{1}{2} \frac{dm}{dt} v^2$$

Initial momentum $p = m v$

Final momentum $p' = (M + dm) v$

$$F = \frac{dp}{dt} = \frac{dm}{dt} v;$$

($\Delta p = dm v$; $\Delta P = F \Delta t$)

$$\frac{dW}{dt} = F \cdot v = \frac{d}{dt} (m v^2);$$

2.6 Velocity phase space and phase portraits

- N particles
- $6N$ variables
- $3N$ coordinates
- $3N$ velocities

$$v(x) = -A \cos x; \quad A > 0, \quad -\infty < x < \infty;$$

$$E = \frac{1}{2} m \dot{x}^2 + v(x) = \frac{1}{2} m \dot{x}^2 - A \cos x = \frac{1}{2} m v^2 - A \cos x;$$

For $E > A$, the motion takes place entirely within one of the wells

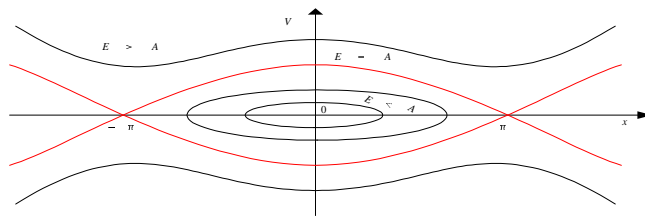
$$p_{\text{Period}} = \sqrt{2m} \int_{x_1}^{x_2} \frac{dx}{\sqrt{E - v(x)}} = \int_{x_1}^{x_2} \frac{dx}{\sqrt{E + A \cos x}};$$

$$x_{1,2} = \pm \cos^{-1} \left(\frac{E}{A} \right)$$

$$F = -\frac{dv}{dx};$$

$$E = A;$$

$$v = \pm \sqrt{\frac{2}{m} (E + A \cos x)}$$



(v, x) **velocity phase space**

Such a graph is called **phase portrait** of the dynamical system

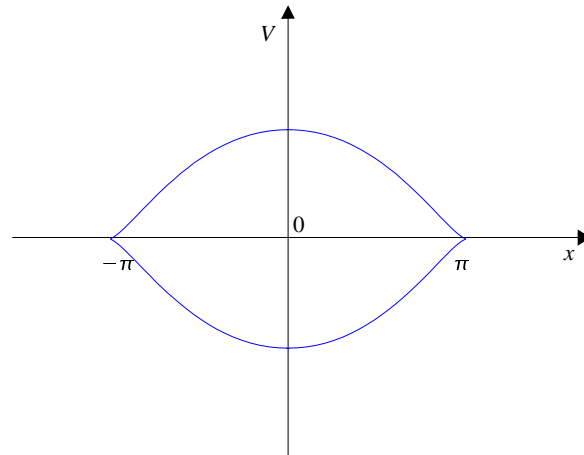
x near 0:

$$v(x) = v(0) + x v'(0) + \frac{1}{2} x^2 v''(0) + \dots \approx A \left(-1 + \frac{1}{2} x^2 + \dots \right);$$

$$\frac{m v^2}{2(E + A)} + \frac{A x^2}{2(E + A)} = 1;$$

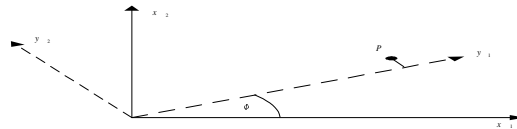
Separatrix: the curve corresponding to $E = A$ separates the bounded motion from the unbounded one.

Separatrix consists of 4 orbits for $x \in [-\pi, \pi]$.



2.7 Rotating frames

Inertial frame



Rotation around $x_3 = y_3$

Inertial frame: (x_1, x_2, x_3)

Rotating frame: (y_1, y_2, y_3)

$$\frac{d\phi}{dt} = \omega = \text{const}$$

(ω : angular velocity)

$\vec{\omega}$ angular velocity vector

$$|\vec{\omega}| = \omega$$

$\vec{\omega} \parallel$ axis of rotation

$$\phi = \omega t + \phi_0, \text{ and we set } \phi_0 = 0; \phi = \omega t$$

$$\begin{pmatrix} y_1 \\ y_2 \\ y_3 \end{pmatrix} = \begin{pmatrix} \cos \omega t & -\sin \omega t & 0 \\ \sin \omega t & \cos \omega t & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix}$$

$$y_1 = x_1 \cos \omega t - \sin \omega t x_2$$

$$y_2 = x_1 \sin \omega t + \cos \omega t x_2$$

$$y_3 = x_3$$

Free particle: $\ddot{\vec{x}} = 0$ in inertial frame

$$\dot{y}_1 = \dot{x}_1 \cos \omega t - \dot{x}_2 \sin \omega t - \omega y_2$$

$$\dot{y}_2 = \dot{x}_1 \sin \omega t + \dot{x}_2 \cos \omega t + \omega y_1$$

$$\dot{y}_3 = \dot{x}_3$$

$$\ddot{y}_1, \ddot{y}_2, \ddot{y}_3 = ?$$

Using $\ddot{x}_1 = \ddot{x}_2 = \ddot{x}_3 = 0$:

$$\ddot{y}_1 = \omega (-\dot{x}_1 \sin \omega t - \dot{x}_2 \cos \omega t) - \omega \dot{y}_2 = -\omega (\dot{y}_2 - \omega y_1) - \omega \dot{y}_2 = \omega^2 y_1 - 2 \omega \dot{y}_2 ;$$

$$\ddot{y}_2 = \omega (\dot{x}_1 \cos \omega t - \dot{x}_2 \sin \omega t) + \omega \dot{y}_1 = \omega (\dot{y}_1 + \omega y_2) + \omega \dot{y}_1 = \omega^2 y_2 + 2 \omega \dot{y}_1 ;$$

$$\ddot{y}_3 = 0 ;$$

$$\ddot{\vec{y}} = \vec{\omega} \times (\vec{\omega} \times \vec{y}) + 2 \vec{\omega} \times \dot{\vec{y}}$$

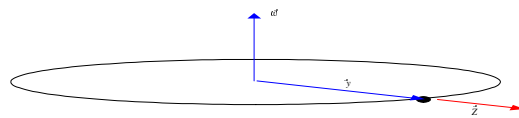
$\vec{\omega}$ is angular velocity vector, of magnitude ω , pointing along the rotation axis.

$$\vec{F} = -m \ddot{\vec{y}} = \vec{Z} + \vec{C}$$

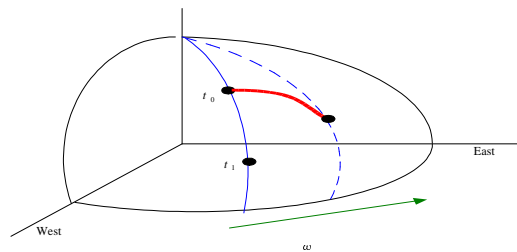
$$\vec{Z} = -m \vec{\omega} \times (\vec{\omega} \times \vec{y}) \quad \text{centrifugal force}$$

$$\vec{C} = -2 m \vec{\omega} \times \dot{\vec{y}} \quad \text{coriolis force}$$

„fictitious forces“



Rotating Earth: $|\vec{Z}| \sim 0.3 \%$ of the gravitational force at the equator



Plane: moves strictly along a meridian at constant height and speed in inertial frame

2.8 The Lorentz force

The electric field at \vec{x} due to a point charge q_i at \vec{x}_i is given by **Coulomb's law** :

$$\vec{E}(\vec{x}) = k q_i \frac{(\vec{x} - \vec{x}_i)}{|\vec{x} - \vec{x}_i|^3}$$

$\vec{E}(\vec{x})$ is the force per unit charge acting at \vec{x} :

$$\vec{F}(\vec{x}) = q_2 \vec{E}(\vec{x})$$

$$k = (4 \pi \epsilon_0)^{-1} ,$$

$$\epsilon_0 = 8.854 \cdot 10^{-12} \frac{\text{Farad}}{\text{meter}}$$

permittivity of free space

$$\vec{E}(\vec{x}) = -\vec{\nabla} \phi(\vec{x})$$

$$\phi(\vec{x}) = -k q_i \frac{1}{|\vec{x} - \vec{x}_i|}$$

A continuous charge distribution $\rho(\vec{x})$

$$\vec{E}(\vec{x}) = k \int \rho(\vec{x}') \frac{(\vec{x} - \vec{x}')}{|\vec{x} - \vec{x}'|^3} d^3 x'$$

$$\phi(\vec{x}) = k \int \frac{\rho(\vec{x}')}{|\vec{x} - \vec{x}'|} d^3 x'$$

Maxwell's equations for static electric fields:

$$\text{Theorem 1 (Gauss's law)} : \epsilon_0 \vec{\nabla} \cdot \vec{E}(\vec{x}) = \epsilon_0 \text{div } \vec{E}(\vec{x}) = \rho(\vec{x})$$

$$\text{Theorem 2} : \vec{\nabla} \times \vec{E}(\vec{x}) = \text{curl } \vec{E}(\vec{x}) = 0$$

Proof:

Definition: The **Laplace operator** or **Laplacian** is defined by:

$$\Delta \equiv \vec{\nabla} \cdot \vec{\nabla} \equiv \text{div grad} \quad \underset{\text{cartesian coordinates}}{=} \quad \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}$$

Definition: The δ -function is a special type of function, called functional or distribution, with following properties:

$$\delta(\vec{x}) = \begin{cases} 0 & \vec{x} \neq 0 \\ \infty & \vec{x} = 0 \end{cases}$$

such that

$$\int f(\vec{x}) \delta(\vec{x}) d^3 x = f(0)$$

for any continuous and integrable function $f(\vec{x})$.

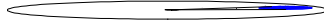
$$\Delta \left(\frac{1}{r} \right), \quad r = |\vec{x}| = \sqrt{x^2 + y^2 + z^2};$$

$$\begin{aligned} \Delta \left(\frac{1}{r} \right) &= \vec{\nabla} \cdot \left(-\frac{\vec{r}}{r^3} \right) = \frac{\partial}{\partial x} \left(\frac{-x}{r^3} \right) + \frac{\partial}{\partial y} \left(\frac{-y}{r^3} \right) + \frac{\partial}{\partial z} \left(\frac{-z}{r^3} \right) \\ &= \left(3 \frac{x^2}{r^5} - \frac{1}{r^3} \right) + \left(3 \frac{y^2}{r^5} - \frac{1}{r^3} \right) + \left(3 \frac{z^2}{r^5} - \frac{1}{r^3} \right) = 0 \end{aligned}$$

for $r \neq 0$.

$r = 0$ case: Integrate over a small volume V containing the origin and apply Gauss's integral theorem:

$$\int_V \nabla^2 \left(\frac{1}{r} \right) d^3 x = \int_V \vec{\nabla} \cdot \vec{\nabla} \left(\frac{1}{r} \right) d^3 x \stackrel{\text{Gauss}}{=} \int_S \vec{n} \cdot \vec{\nabla} \left(\frac{1}{r} \right) dS$$



$$dS = r^2 d\Omega;$$

$$d\Omega = \text{space angle} = \sin \theta d\phi d\theta;$$

$$V = \frac{4\pi r^3}{3};$$

$$\int_S \vec{n} \cdot \vec{\nabla} \left(\frac{1}{r} \right) dS = \int_S \underbrace{\frac{\partial}{\partial r} \left(\frac{1}{r} \right)}_{-\frac{1}{r^2}} r^2 d\Omega = - \int_S d\Omega = -4\pi;$$

$$\int_0^\pi \sin \theta d\theta \int_0^{2\pi} d\phi = 4\pi;$$

$$\Delta \left(\frac{1}{|\vec{x} - \vec{x}'|} \right) = -4\pi \delta(\vec{x} - \vec{x}');$$

$$\vec{\nabla} \cdot \vec{E}(\vec{x}) = -\Delta \phi(\vec{x}) = -k \int d^3x' \rho(\vec{x}') \Delta \left(\frac{1}{|\vec{x} - \vec{x}'|} \right) = 4\pi k \rho(\vec{x});$$

Magnetic fields: One never finds isolated magnetic charges or „monopoles“, only dipoles.

Absence of magnetic monopoles:

$$\begin{aligned} \vec{\nabla} \cdot \vec{B}(\vec{x}) &= 0; \\ \text{div } \vec{B}(\vec{x}) &= 0; \end{aligned}$$

$$\text{div curl } \vec{A} \equiv 0 \Rightarrow \vec{B}(\vec{x}) = \vec{\nabla} \times \vec{A}(\vec{x})$$

$\vec{A}(\vec{x})$: vector potential

$\vec{A}(\vec{x})$ is not unique, since

$$\vec{A}(\vec{x}) \rightarrow \vec{A}(\vec{x}) + \vec{\nabla} \Lambda(\vec{x})$$

$\vec{B}(\vec{x})$ does not change (curl grad $\Lambda \equiv 0$)

Such a transformation is called **gauge transformation**.

The total electromagnetic force on a charged particle with charge q is:

$$\vec{F} = q (\vec{E} + \vec{v} \times \vec{B}) \quad (\text{Lorentz force})$$

This force is conservative, $\int \vec{F} d\vec{x} = 0$, since \vec{v} is tangent to trajectory.

Supplement: What is the difference between experimental and theoretical physics?

Theory: Develops mathematical schemes to solve dynamical equations. Focuses on predictions of a system's dynamical behavior, based on postulated fundamental laws.

Experiment: Develops reproducible, accurate measurement techniques. Focuses on measurements of a system's dynamical behavior, in order to check the theoretical

predictions, with the ultimate goal to check and to reduce the number of fundamental laws.

3.Lagrangianformulationofmechanics

Sometimes a particle is not free to move in Euclidean 3-space but only in a *restricted* region. Such a system is called a **constrained system**. The particle's area of motion, **configuration manifold**, is neither Euclidean nor 3N-dimensional.

⇒ Equations of motion must include information about the forces that give rise to the constraints.

How Newton's equations can be rewritten such that constraints are taken into account from the outset ⇒ **Lagrangian formulation of dynamics** .

Lagrange equations

- same physical content as Newton's equations
- easier to apply to dynamical systems
- symmetry
- variational principle

3.1 Constraints and configuration manifolds

3.1.1 Constraints and work

The motion is often constrained by some external agents applying forces that are initially unknown (body gliding on a table, a swinging weight of a pendulum).

Suppose one is dealing with a system of N particles and that the constraints are given by **constraint equations** :

$$f_j(\vec{x}_1, \dots, \vec{x}_N, t) = 0; \quad j = 1, 2, \dots, K < 3N; (1)$$

\vec{x}_i are position vectors of the N particles. The f_j are differentiable functions. t -dependence: e.g. surface of a table could be wavy.

Constraints of type (1) are called **holonomic** (means integrable).

More general:

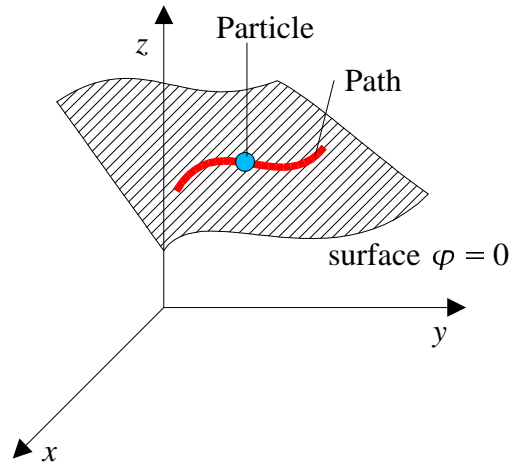
$$f_j(\vec{x}_1, \dots, \vec{x}_N, \dot{\vec{x}}_1, \dots, \dot{\vec{x}}_N, t) = 0; \quad j = 1, \dots, K < 3N$$

called **non-holonomic**.

Other:

$$f_j(\vec{x}_1, \dots, \vec{x}_N, t) < 0$$

Example: 1 particle $N = 1$; 1 constraint $K = 1$



$$m \ddot{\vec{x}} = \vec{F} + \vec{C}$$

$\vec{F}(\vec{x}, \dot{\vec{x}}, t)$ known external force

\vec{C} unknown force of constraint that the surface exerts on particle.

\vec{C} force that ensures the particle to stay on $f = 0$ but otherwise to pose no restriction for the particle

$\vec{C} \perp$ surface $f = 0$

$f(\vec{x}, t) = \text{const}$ be the equation of any surface $\Rightarrow \vec{\nabla} f(\vec{x}, t) \perp$ surface provided $\vec{\nabla} f \neq 0$:

$\vec{\nabla} f \neq 0$ on the $f=0$ surface

Example: $f_a(\vec{x}) = \vec{s} \cdot \vec{x} = 0$

$$f_b(\vec{x}) = (\vec{s} \cdot \vec{x})^2 = 0$$

$\vec{\nabla} f_a = \vec{s}$ whereas $\vec{\nabla} f_b = 0$

\Rightarrow only $f_a = 0$ is acceptable

If $N > 1, K > 1$, the matrix $\left\{ \frac{\partial f_j}{\partial x^\alpha} \right\}$; $\alpha = 1, \dots, 3N$; $j = 1, \dots, K$ be at least of rank K .

$\vec{C} = \lambda \vec{\nabla} f(\vec{x}, t)$ $\lambda = \lambda(t)$ can be any number.

$$\left. \begin{aligned} m \ddot{\vec{x}} &= \vec{F} + \vec{C} \\ f(\vec{x}, t) &= 0 \end{aligned} \right\} \begin{array}{l} x(t) \\ y(t) \\ z(t) \end{array}$$

unknowns: $x(t), y(t), z(t), \lambda$

4 equations for 4 unknowns

\vec{C} is also called **normal force**.

Assume that the external force:

$$\vec{f} = -\vec{\nabla} V(\vec{x}, t)$$

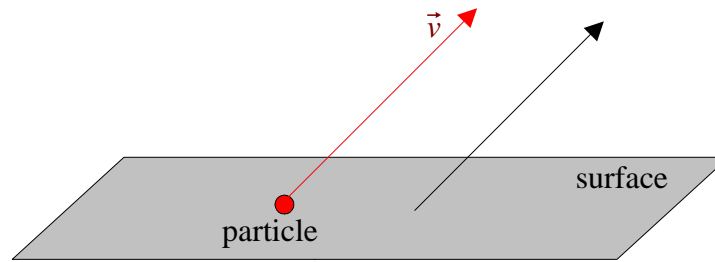
$$m \ddot{\vec{x}} \cdot \dot{\vec{x}} \equiv \frac{d}{dt} \left(\frac{1}{2} m \dot{\vec{x}}^2 \right) = -\vec{\nabla} V \cdot \dot{\vec{x}} + \lambda \vec{\nabla} f \cdot \dot{\vec{x}}$$

$$f(\vec{x}(t), t) = 0$$

$$\frac{df}{dt} = \vec{\nabla} f \cdot \dot{\vec{x}} + \frac{\partial f}{\partial t} = 0$$

$$\frac{dV}{dt} = \vec{\nabla} V \cdot \dot{\vec{x}} + \frac{\partial V}{\partial t}$$

$$\frac{dE}{dt} = \frac{d}{dt} \left[\frac{1}{2} m \dot{\vec{x}}^2 + V \right] = \frac{\partial V}{\partial t} - \delta \cdot \frac{\partial f}{\partial t}$$



If the surface moves, the particle on it also moves.

Thus: For static surfaces $\left(\frac{\partial f}{\partial t} = 0\right)$ constraint forces do no work!

Friction: Here: Only constraint forces that $\propto \vec{\nabla} f$

3.1.2 Generalized coordinates

$$m \ddot{\vec{x}} = \vec{F} + \lambda \vec{\nabla} f$$

$$f(\vec{x}, t) = 0$$

Choose: **arbitrary** vector $\vec{\tau}$ tangent to the surface $f=0$, i.e. $\vec{\tau} \cdot \vec{\nabla} f = 0$

$$(m \ddot{\vec{x}} - \vec{F}) \cdot \vec{\tau} = 0 (*)$$

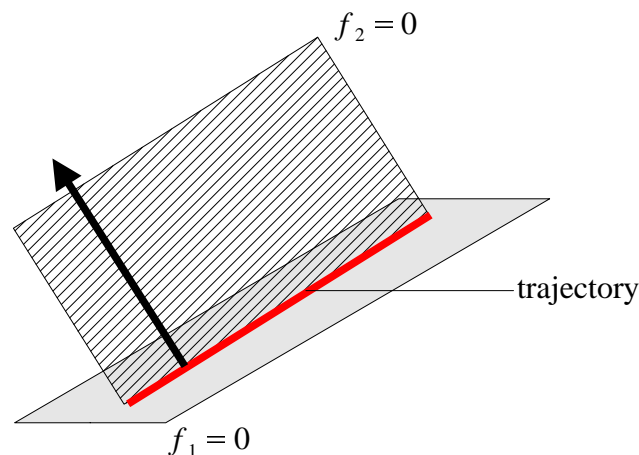
\Rightarrow 2 linearly independent vectors at each point \vec{x} and hence 2 linearly independent vector functions of \vec{x} and that describe a tangent to the surface.

(*) yields 2 equations for $\vec{x}(t) + f(\vec{x}, t) = 0 \dots 3^{\text{rd}}$ equation. $\vec{\tau} \cdot \vec{\nabla} f = 0$

1 particle in 3D-space can have at most 2 holonomic constraints.

$$f_1(\vec{x}, t) = 0 ; \quad f_2(\vec{x}, t) = 0$$

$$\vec{C} = \lambda_1 \vec{\nabla} f_1 + \lambda_2 \vec{\nabla} f_2$$



System of N particles: K independent holonomic constraints. We drop the summation convention for this section.

$$m_i \ddot{\vec{x}}_i = \vec{F}_i + \vec{C}_i$$

$$\vec{C}_i = \sum_{j=1}^K \lambda_j \vec{\nabla}_i f_j$$

$$\frac{\partial V}{\partial t} = 0 \Rightarrow \frac{dE}{dt} = - \sum_j \lambda_j \frac{\partial f_j}{\partial t}$$

Now let $\vec{\tau}_i$ be N arbitrary vectors, tangent to the surface: $\sum_{i=1}^N \vec{\tau}_i \vec{\nabla}_i f_j = 0 ; j = 1, \dots, K$

If $\frac{\partial f_j}{\partial x^\alpha}$ is of rank K , this equation gives K independent relations among the $3N$ components of the

N vectors $\vec{\tau}_i$ so that $3N - K$ of the components $\vec{\tau}_i$ are independent.

$$\sum_i (m_i \dot{\vec{x}}_i - \vec{F}_i) \cdot \vec{\tau}_i = 0$$

D'Alembert's principle:

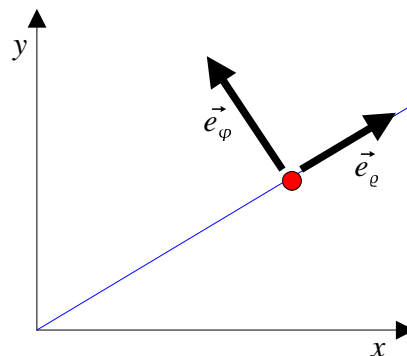
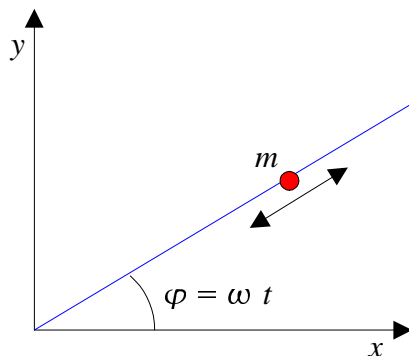
$3N - K$ independent components of $\vec{\tau}_i$.

$3N - K$ independent relations. $f_j = 0 (j = 1 \dots K)$ provide K other relations.

The dynamical system is constrained to a $(3N - K)$ -dimensional hypersurface: Configuration manifold \mathcal{Q} of the system.

The problem is to pick the $3N - K$ components of the $\vec{\tau}_i$ that fully characterize the motion in \mathcal{Q}

Example: A particle moves along a rigid rod that rotates with a given angular velocity ω .



$$f_1 = z = 0$$

$$f_2 = \arctan\left(\frac{y}{x}\right) - \omega t = 0$$

$z = \dot{z} = \ddot{z} = 0 \Rightarrow$ eliminate z -coordinates all together

$$\left. \begin{array}{l} x = \rho \cos \varphi \\ y = \rho \sin \varphi \end{array} \right\} \Rightarrow f_2 = \varphi - \omega t = 0$$

The equation of motion is $m \ddot{\vec{x}} = \lambda \text{grad } f_2$

$$\text{grad} = \vec{e}_\rho \frac{\partial}{\partial \rho} + \vec{e}_\varphi \frac{1}{\rho} \frac{\partial}{\partial \varphi}$$

$$\ddot{\vec{x}} = (\ddot{\rho} - \rho \dot{\varphi}^2) \vec{e}_\rho + (\rho \ddot{\varphi} + 2 \dot{\rho} \dot{\varphi}) \vec{e}_\varphi$$

$$\text{grad } f_2 = \vec{e}_\varphi \frac{1}{\rho}$$

Component along \vec{e}_ρ : $m \ddot{\rho} - m \rho \dot{\varphi}^2 = 0$

Component along \vec{e}_φ : $m \rho \ddot{\varphi} + 2 m \dot{\rho} \dot{\varphi} = \frac{\lambda}{\rho}$

The projection $(m \ddot{\vec{x}} - \lambda \text{grad } f_2) \cdot \vec{\tau} = m \ddot{\vec{x}} \cdot \vec{\tau} = 0$ ($\vec{\tau} \propto \vec{e}_\rho$)

is $m \ddot{\rho} - m \omega^2 \rho = 0$ since $\varphi = \omega t \Rightarrow \dot{\varphi} = \omega$.

Is a linear homogeneous ODE with constant coefficients $\rightarrow \rho(t) \propto e^{\kappa t}$

$$\rho(t) = A e^{\omega t} + B e^{-\omega t}$$

General solution:

$$(*) \quad \dot{\varphi} = \omega, \quad \ddot{\varphi} = 0$$

$$z. \quad m \dot{\rho} = \frac{\lambda}{\rho}$$

$$\vec{C} = \lambda \text{grad } f_2 = 2 m \omega^2 \vec{e}_\varphi (A e^{\omega t} - B e^{-\omega t})$$

Now we return to our N-particle problem: Picking the $\vec{\tau}_i$ to satisfy:

$$\sum_{i=1}^N \vec{\tau}_i \cdot \vec{\nabla}_i f_j = 0 \quad (j = 1, \dots, K)$$

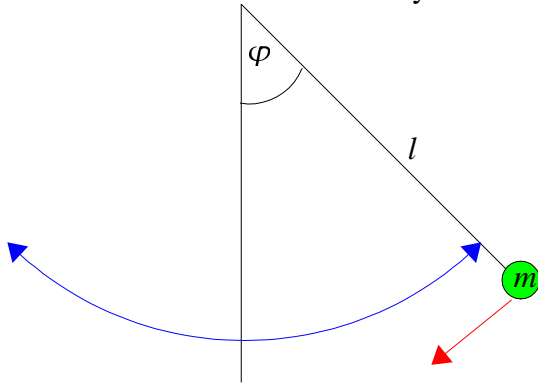
means picking the generalized tangent vector with $3N - K$ independent components.

Define $3N - K$ generalized coordinates q^{α} , $\alpha = 1, \dots, 3N - K$ such that they uniquely determine all particle coordinates $\vec{x}_i = \vec{x}_i(q^1, q^2, \dots, q^{3N-K}, t)$ $i = 1, \dots, N$ and guarantee the equations of constraint to be obeyed for **any** values of q^α ,

$$f_j(\vec{x}_1(q^1 \dots q^f, t), \vec{x}_2(q^1 \dots q^f, t), \dots, \vec{x}_N(q^1 \dots q^f, t)) = 0$$

$$f_j(x_1(q^1 \dots q^f, t), \dots, x_{3N}(q^1 \dots q^f, t)) = 0 \text{ for arbitrary } \{q^\alpha\} \text{ and for } j = 1, \dots, K \text{ where } f = 3N - K$$

is the number of freedoms of the system.



$$i = 1, \dots, N$$

$$m_i \ddot{\vec{x}}_i = \vec{F}_i + \vec{C}_i;$$

$$f_j(\vec{x}_1, \dots, \vec{x}_N, t) = 0 \quad j = 1, \dots, K;$$

$$\vec{C}_i = \sum_{j=1}^K \lambda_j \vec{\nabla}_i f_j$$

$$\sum_{i=1}^N \vec{\tau}_i \cdot \vec{\nabla}_i f_j = 0 \quad j = 1, \dots, K$$

$$\sum_{i=1}^N (m_i \ddot{\vec{x}}_i - \vec{F}_i) \cdot \vec{\tau}_i = 0$$

Generalized Coordinates:

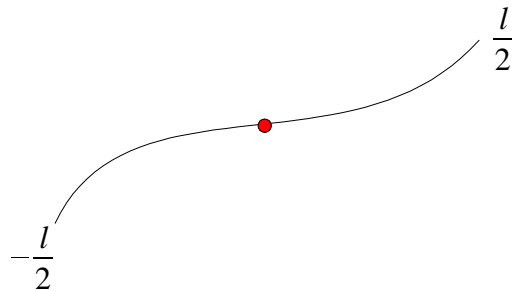
$$q^\alpha : \alpha = 1, \dots, 3N - K$$

- $\vec{x}_i = \vec{x}_i(q^1, q^2, \dots, q^{3N-K}, t) \quad i = 1, \dots, N$
- $f_j(\vec{x}_1(q^1, \dots, q^n, t), \vec{x}_2(q^1, \dots, q^n, t), \dots, \vec{x}_N(q^1, \dots, q^n, t)) = 0$
 $n = 3N - K$ for any $\{q^\alpha\} \wedge j = 1, \dots, K$

3.1.3 Examples of configuration manifolds

Greek indices run from 1 to $n = 3N - K$

The finite line



Motion of bead along wire.

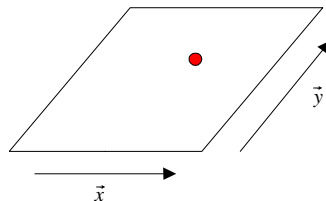
$$N = 1, K = 2 \Rightarrow n = 1;$$

Dimension of $\mathbb{Q} = 1$

Generalized coordinate: $-l/2 \leq q \leq l/2$

The plane

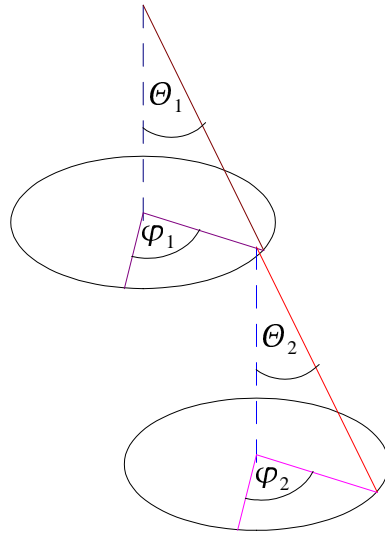
Particle on a table: $N = 1, K = 1 \Rightarrow n = 2;$



$$q^1 = x, q^2 = y;$$

The Double Pendulum

Spherical pendulums suspended from another are:



$N = 2, K = 2; 3 \cdot 2 - 2 = 4 \Rightarrow \dim \mathbb{Q} = 4$

$q^\alpha : \phi_1, \phi_2, \theta_1, \theta_2$

3.2 Lagrange's Equations

3.2.1 Derivation of Lagrange's Equations

$$\sum_{i=1}^N (m_i \ddot{\vec{x}}_i - \vec{F}_i) \cdot \vec{\tau}_i = 0$$

$\ddot{\vec{x}}_i, \vec{F}_i$ and $\vec{\tau}_i$ use q^α

Notation: We will use the summation convention for greek indices ($1 \dots n = 3N - K$), but we continue to use summation signs for $i = 1 \dots n$.

Corollary: $\vec{\tau}_i = \varepsilon^\alpha \frac{\partial \vec{x}_i(q^1, \dots, q^n, t)}{\partial q^\alpha}$
 where ε^α are arbitrary constants ($\alpha = 1 \dots n$).

Proof: (1) $f_j(q^1, \dots, q^n, t) = 0$ must be obeyed for any value of $\{q^\alpha\}$.

$$\frac{\partial f_j}{\partial q^\alpha} \equiv 0$$

$$(2) \sum_{i=1}^N \vec{\tau}_i \cdot \vec{\nabla}_i f_j = \varepsilon^\alpha \sum_{i=1}^N \vec{\nabla}_i f_j \frac{\partial \vec{x}_i}{\partial q^\alpha} = \varepsilon^\alpha \frac{\partial f_j}{\partial q^\alpha} \stackrel{(1)}{=} 0.$$

Choose: $\{\varepsilon^\alpha\} = \{1, 0, 0, \dots\}, \{0, 1, 0, \dots\}, \dots$:

$$\sum_{i=1}^N (m_i \ddot{\vec{x}}_i - \vec{F}_i) \frac{\partial \vec{x}_i}{\partial q^\alpha} = 0 \quad \alpha = 1, \dots, n;$$

$$\vec{F}_i = -\nabla V(\vec{x}_1, \dots, \vec{x}_N);$$

$$\sum_{i=1}^N \vec{F}_i \cdot \frac{\partial \vec{x}_i}{\partial q^\alpha} = - \sum_{i=1}^N \vec{\nabla}_i V \cdot \frac{\partial \vec{x}_i}{\partial q^\alpha} = - \frac{\partial V}{\partial q^\alpha};$$

$$\ddot{\vec{x}}_i \cdot \frac{\partial \vec{x}_i}{\partial q^\alpha} = \frac{d}{dt} \left[\dot{\vec{x}}_i \cdot \frac{\partial \vec{x}_i}{\partial q^\alpha} \right] - \dot{\vec{x}}_i \cdot \frac{d}{dt} \left(\frac{\partial \vec{x}_i}{\partial q^\alpha} \right);$$

$$\vec{v}_i \equiv \dot{\vec{x}}_i = \frac{d \vec{x}_i}{dt} = \frac{\partial \vec{x}_i}{\partial q^\alpha} \dot{q}^\alpha + \frac{\partial \vec{x}_i}{\partial t};$$

$$\frac{\partial \vec{v}_i}{\partial \dot{q}^\alpha} \equiv \frac{\partial \dot{\vec{x}}_i}{\partial \dot{q}^\alpha} = \frac{\partial \vec{x}_i}{\partial q^\alpha};$$

$$\frac{d}{dt} \left(\frac{\partial \vec{x}_i}{\partial q^\alpha} \right) = \frac{\partial^2 \vec{x}_i}{\partial q^\alpha \partial q^\beta} \cdot \dot{q}^\beta + \frac{\partial}{\partial t} \left(\frac{\partial \vec{x}_i}{\partial q^\alpha} \right) = \frac{\partial}{\partial q^\alpha} \left(\frac{\partial \vec{x}_i}{\partial q^\beta} \dot{q}^\beta + \frac{\partial \vec{x}_i}{\partial t} \right) = \frac{\partial \vec{v}_i}{\partial q^\alpha};$$

$$\sum_{i=1}^N m_i \ddot{\vec{x}}_i \cdot \frac{\partial \vec{x}_i}{\partial q^\alpha} = \sum_{i=1}^N \left[\frac{d}{dt} \left(m_i \vec{v}_i \cdot \frac{\partial \vec{v}_i}{\partial \dot{q}^\alpha} \right) - m_i \vec{v}_i \cdot \frac{\partial \vec{v}_i}{\partial q^\alpha} \right] = \frac{d}{dt} \left(\frac{\partial T}{\partial \dot{q}^\alpha} \right) - \frac{\partial T}{\partial q^\alpha}$$

$$T = \frac{1}{2} \sum_{i=1}^N m_i v_i^2;$$

$$\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{q}^\alpha} \right) - \frac{\partial T}{\partial q^\alpha} + \frac{\partial V}{\partial q^\alpha} = 0 \quad \alpha = 1, \dots, n$$

$$\frac{\partial V}{\partial \dot{q}^\alpha} = 0;$$

$$(V = V(q^\alpha))$$

$$L = T - V:$$

LagrangianfunctionorsimplyLagrangian $L(q^\alpha, \dot{q}^\alpha, t)$:

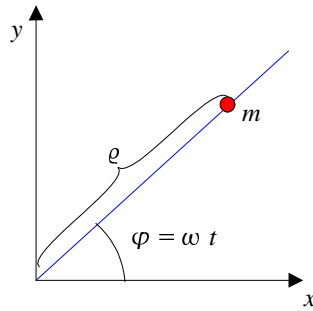
$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}^\alpha} \right) - \frac{\partial L}{\partial q^\alpha} = 0 \quad \alpha = 1, \dots, n = 3N - K;$$

Like Newtons' equations, Lagranges' equations are a set of 2nd-order equations, but now for the $q^\alpha(t)$.

$$\frac{\partial^2 L}{\partial \dot{q}^\beta \partial \dot{q}^\alpha} \ddot{q}^\beta + \frac{\partial^2 L}{\partial q^\beta \partial \dot{q}^\alpha} \dot{q}^\beta + \frac{\partial^2 L}{\partial t \partial \dot{q}^\alpha} - \frac{\partial L}{\partial q^\alpha} = 0;$$

3.2.2Examples

1.:



$$q = \varrho$$

$$x = \varrho \cos \omega t$$

$$y = \varrho \sin \omega t$$

$$z = 0$$

$$V = 0$$

$$L(\varrho, \dot{\varrho}) = T = \frac{m}{2} (\dot{x}^2 + \dot{y}^2 + \dot{z}^2);$$

$$\dot{x} = \dot{\varrho} \cos \omega t - \varrho \omega \sin \omega t;$$

$$\dot{y} = \dot{\varrho} \sin \omega t + \varrho \omega \cos \omega t;$$

$$L(\varrho, \dot{\varrho}) = \frac{m}{2} (\dot{\varrho}^2 + \omega^2 \varrho^2);$$

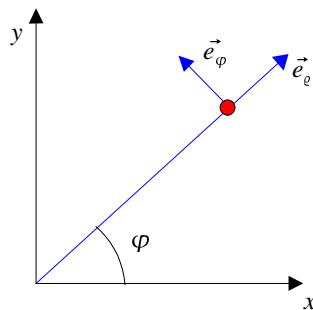
$$\frac{\partial L}{\partial \dot{\varrho}} = m \dot{\varrho}, \quad \frac{\partial L}{\partial \varrho} = m \omega^2 \varrho;$$

$$\ddot{\varrho} - \omega^2 \varrho = 0;$$

Oldway :

$$f_1 = z = 0;$$

$$f_2 = \underbrace{\arctan\left(\frac{y}{x}\right)}_{\varphi} - \omega t = 0$$



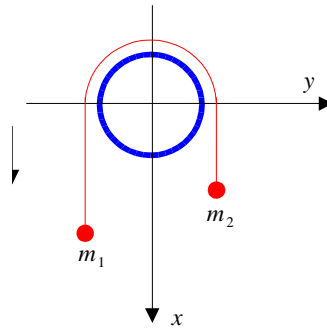
$$m \ddot{\vec{x}} = \lambda \underbrace{\text{grad } f_2}_{=\vec{c}};$$

$$\vec{C} = 2 m \omega^2 \vec{e}_\varphi (A e^{\omega t} - B e^{-\omega t});$$

$$\varrho(t) = A e^{\omega t} + B e^{-\omega t};$$

2.:

Two particles m_1 , m_2 are connected by an inextensible string of negligible mass and of length l which passes over a frictionless pulley of negligible mass.



$$q = x_1 \text{ (1 degree of freedom)}$$

$$x_1 = q, y_1 = -R, z_1 = 0;$$

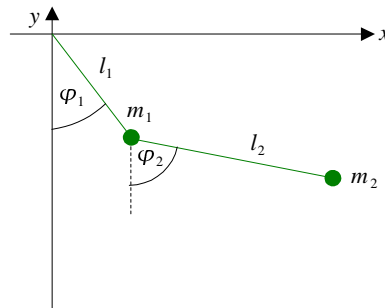
$$x_2 = l - q, y_2 = R, z_2 = 0$$

$$T = \frac{1}{2} (m \dot{x}_1^2 + m_2 \dot{x}_2^2) = \frac{1}{2} (m_1 + m_2) \dot{q}^2;$$

$$V = -m_1 g x_1 - m_2 g x_2 = -m_1 g q - m_2 g (l - q) = -g (m_1 - m_2) q + \text{const};$$

$$L(q, \dot{q}) = \frac{1}{2} (m_1 + m_2) \dot{q}^2 + q (m_1 - m_2) g \Rightarrow (m_1 + m_2) \ddot{q} = (m_1 - m_2) g;$$

3. Planar Double Pendulum :



$$x_1 = l_1 \sin \varphi_1$$

$$y_1 = -l_1 \cos \varphi_1$$

$$z_1 = 0;$$

$$x_2 = l_1 \sin \varphi_1 + l_2 \sin \varphi_2;$$

$$y_2 = -l_1 \cos \varphi_1 - l_2 \cos \varphi_2$$

$$z_2 = 0$$

$$T = \frac{m_1}{2} (\dot{x}_1^2 + \dot{y}_1^2) + \frac{m_2}{2} (\dot{x}_2^2 + \dot{y}_2^2) = \frac{m_1}{2} l_1^2 \dot{\varphi}_1^2 + \frac{m_2}{2} (l_1^2 \dot{\varphi}_1^2 + l_2^2 \dot{\varphi}_2^2 + 2 l_1 l_2 \cos(\varphi_1 - \varphi_2) \dot{\varphi}_1 \dot{\varphi}_2)$$

;

$$V = m_1 g y_1 + m_2 g y_2 = -(m_1 + m_2) g l_1 \cos \varphi_1 - m_2 g l_2 \cos \varphi_2;$$

$$L = T - V;$$

3.2.3 Transformations and Conservation of Energy

Theorem: Let L_1 and L_2 be two Lagrangian functions such that the equations of motion obtained from them are *exactly* the same. Then there exists a function ϕ on the configuration manifold \mathbb{Q} such that

$$L_1 - L_2 = \frac{d\phi}{dt}.$$

Proof: Jose and Saletan.

$$\frac{\partial^2 L}{\partial \dot{q}^\beta \partial \dot{q}^\alpha} \ddot{q}^\beta = G_\alpha(q, \dot{q}, t)$$

Take $q(t_0), \dot{q}(t_0)$: Hessian Condition

$$\det \left(\underbrace{\frac{\partial^2 L}{\partial \dot{q}^\alpha \partial \dot{q}^\beta}}_{\text{Hessian Matrix}} \right) \neq 0$$

Problem: Given $L \Rightarrow E = T + V$?

Single particle, cartesian coordinates:

$$\frac{\partial V}{\partial \dot{x}} = 0$$

$$T = \frac{1}{2} m \dot{x}^2 \Rightarrow \dot{x} \frac{\partial L}{\partial \dot{x}} - L = \underbrace{\dot{x} \frac{\partial T}{\partial \dot{x}}}_{2T} - T + V = T + V = E$$

General case:

$$E(q, \dot{q}) \equiv \dot{q}^\alpha \frac{\partial L}{\partial \dot{q}^\alpha} - L$$

$$\dot{E} = \frac{d}{dt} \left[\dot{q}^\alpha \frac{\partial L}{\partial \dot{q}^\alpha} - L \right] = \ddot{q}^\alpha \frac{\partial L}{\partial \dot{q}^\alpha} + \underbrace{\dot{q}^\alpha \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}^\alpha} \right)}_{\frac{\partial L}{\partial q^\alpha}} - \ddot{q}^\alpha \frac{\partial L}{\partial \dot{q}^\alpha} - \dot{q}^\alpha \frac{\partial L}{\partial q^\alpha} - \frac{\partial L}{\partial t};$$

$$\frac{dE}{dt} = - \frac{\partial L}{\partial t}$$

or

$$\frac{\partial L}{\partial t} = 0 \Rightarrow \frac{dE}{dt} = 0;$$

If $L = T - V$ is time-independent and if $\partial V / \partial \dot{q} = 0 \Rightarrow E = T + V$.

3.2.4 Charged Particle in an Electromagnetic Field

$$\vec{F} = e(\vec{E} + \vec{v} \times \vec{B})$$

In this subsection, use W for energy.

$$F_\alpha = e(E_\alpha + \varepsilon_{\alpha\beta\gamma} v^\beta B_\gamma)$$

$$\varepsilon_{\alpha\beta\gamma} = \begin{cases} 1 & (\alpha\beta\gamma) \text{ is an even cyclic permutation of } (123) \\ -1 & (\alpha\beta\gamma) \text{ is an odd cyclic permutation of } (123) \\ 0 & \text{otherwise} \end{cases}$$

Levi-Civita antisymmetric tensor density

$$\varepsilon_{123} = 1, \quad \varepsilon_{231} = 1, \quad \varepsilon_{321} = -1;$$

$$E_\alpha = -\partial_\alpha \varphi - \partial_t A_\alpha;$$

$$\left(\vec{E} = -\vec{\nabla} \varphi - \frac{\partial \vec{A}}{\partial t} \right);$$

Law of induction

$$B_\alpha = \varepsilon_{\alpha\beta\gamma} \partial_\beta A_\gamma$$

$$(\vec{B} = \text{curl } \vec{A})$$

$$\partial_\alpha \equiv \frac{\partial}{\partial x^\alpha}, \quad \partial_t \equiv \frac{\partial}{\partial t}$$

$$m \ddot{x}^\alpha = -e \partial_\alpha \varphi - e \partial_t A_\alpha + e \varepsilon_{\alpha\beta\gamma} \dot{x}^\beta \varepsilon_{\gamma\mu\nu} \partial_\mu A_\nu$$

$$v^\alpha \equiv \dot{x}^\alpha$$

$$m \dot{v}^\alpha = -e \partial_\alpha \varphi - e \partial_t A_\alpha + e \varepsilon_{\alpha\beta\gamma} v^\beta \varepsilon_{\gamma\mu\nu} \partial_\mu A_\nu$$

$$\varepsilon_{\alpha\beta\gamma} \varepsilon_{\gamma\mu\nu} = \delta_{\alpha\mu} \delta_{\beta\nu} - \delta_{\alpha\nu} \delta_{\beta\mu}$$

$$\left(\delta_{\alpha\beta} = \begin{cases} 1 & \alpha = \beta \\ 0 & \alpha \neq \beta \end{cases} \right)$$

$$m \dot{v}^\alpha = -e \partial_\alpha \varphi - e \partial_t A_\alpha + e (v^\nu \partial_\alpha A_\nu - v^\mu \partial_\mu A_\alpha);$$

$$(\partial_t A_\alpha \text{ und } \partial_\mu A_\alpha : -\frac{d A_\alpha(\vec{x}, t)}{d t})$$

$$\frac{d}{d t} = (m v^\alpha + e A_\alpha) + \partial_\alpha (e \varphi - e v^\nu A_\nu) = 0$$

$$\varphi \text{ does not depend on } v^\alpha, \quad A_\alpha \text{ does not depend on } v^\alpha \Rightarrow$$

$$L = \frac{1}{2} m \dot{x}^2 - e \varphi(\vec{x}, t) + e \dot{x}^\beta A_\beta(\vec{x}, t) = \frac{1}{2} m \dot{x}^2 + e \dot{\vec{x}} \cdot \vec{A}(\vec{x}, t) - e \varphi$$

$$W = \dot{q}^\alpha \frac{\partial L}{\partial \dot{q}^\alpha} - L$$

$$\Rightarrow W = \frac{1}{2} m \dot{x}^2 + e \varphi$$

3.3 Central Force Motion

Consider two bodies (mass points) m_1 and m_2 , interact through a force directed along the line joining them and depends only on distance between the mass points:

$$m_1 \ddot{\vec{x}}_1 = \vec{F}(\vec{x})$$

$$m_2 \ddot{\vec{x}}_2 = -\vec{F}(\vec{x})$$

\vec{F} = force that particle 2 exerts on particle 1 and $\vec{x} = \vec{x}_1 - \vec{x}_2$.

$$\mu \ddot{\vec{x}} = \vec{F}$$

$$\frac{1}{\mu} = \frac{1}{m_1} + \frac{1}{m_2}$$

or

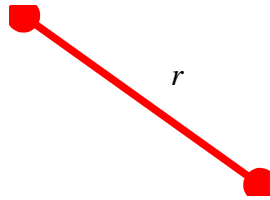
$$\mu = \frac{m_1 m_2}{m_1 + m_2}$$

is **reduced mass**.

The **relativemotion** of the two bodies in a single equation of motion:

$$\vec{F} = -\vec{\nabla} V;$$

$$V = V(|\vec{x}|) \equiv V(r)$$



Angular momentum vector $\vec{J} = \mu \vec{x} \times \dot{\vec{x}}$ is constant. Since \vec{J} is always perpendicular to both \vec{x} and $\dot{\vec{x}}$, \vec{x} lies always in a fixed plane perpendicular to \vec{J} which is determined by the initial conditions.

Choose: $\vec{J} \parallel z$ -axis

$$L = \frac{1}{2} \mu \dot{\vec{x}}^2 - V(r) = \frac{1}{2} \mu (\dot{r}^2 + r^2 \dot{\varphi}^2) - V(r)$$

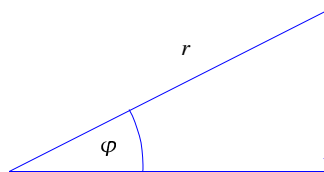
$$[\dot{\vec{x}} = \dot{\varrho} \vec{e}_\varrho + \varrho \dot{\varphi} \vec{e}_\varphi + \dot{z} \vec{e}_z; \dot{z} = 0 \Rightarrow \dot{\vec{x}}^2 = \dot{\varrho}^2 + \varrho^2 \dot{\varphi}^2;]$$

two freedoms: r, φ

$$\text{In addition, } L^{\text{total}} = L^{\text{relative}} + \frac{1}{2} M \dot{X}^2$$

$$\varphi : \frac{d}{dt} (\mu r^2 \dot{\varphi}) = 0$$

$$r : \mu \ddot{r} = \mu r \dot{\varphi}^2 + \frac{dV}{dr} = 0$$



$$v_\perp = r \dot{\varphi}$$

$$l = \mu r v_{\perp} = \mu r^2 \dot{\phi}$$

$$\mu r^2 \dot{\phi} = \text{const} = l = \text{magnitude of } |\vec{J}|$$

$$\mu \ddot{r} - \frac{l^2}{\mu r^3} + \frac{dV}{dr} = 0$$

or

$$\mu \ddot{r} - \frac{d}{dr} \left(\frac{l^2}{2\mu r^2} + V(r) \right) = 0$$

This is equation for a one-dimensional motion of a single particle of mass μ under **effective one-particle potential**.

$$V(r) = \frac{l^2}{2\mu r^2} + V(r)$$

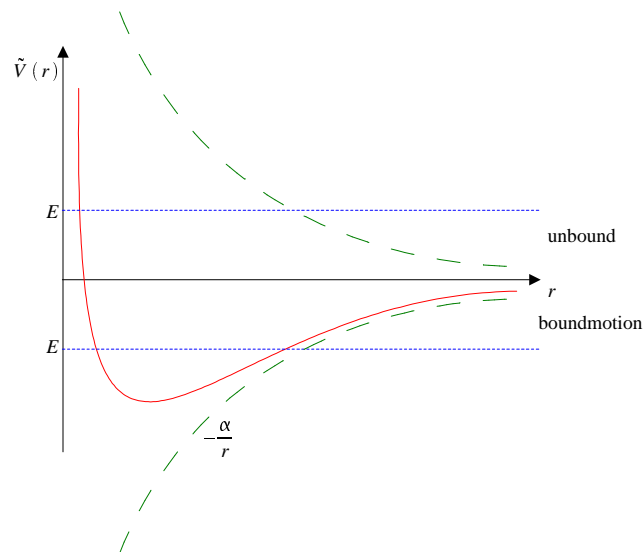
$$\tilde{L}(r) = \frac{1}{2} \mu \dot{r}^2 - \tilde{V}(r)$$

$$\tilde{V}(r) = \frac{l^2}{2\mu r^2} + V(r)$$

equivalent one-dimensional problem

$$V(r) = \frac{-\alpha}{r} \quad (\alpha = G \mu M = G m_1 m_2 \text{ or } \alpha = Z e^2 \text{ for } +Z e \text{ (nucleus) and } -e \text{ (electron)})$$

centrifugal barrier



$$E = T + \tilde{V} = \frac{1}{2} \mu \dot{r}^2 + \frac{l^2}{2\mu r^2} + V(r) = \frac{1}{2} \mu \dot{r}^2 + \frac{1}{2} \mu r^2 \dot{\phi}^2 + V(r) = \text{const};$$

$$E_{\text{orig}} = E + \frac{1}{2} M \dot{X}^2;$$

($\dot{X} = \text{const}$, initial conditions)

3.3.1 The Kepler Problem

Kepler: born in Weilder Stadt

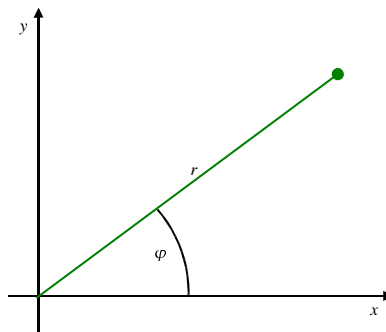
$$V(r) = -\frac{\alpha}{r}, \quad \alpha = G \mu M > 0$$

(K1) the orbit of each planet is an ellipse with the sun at one of its foci

(K2) the position vector from the sun to the planet sweeps out equal areas in equal times

(K3) the period T of each planet's orbit is related to its semimajor axis R so that T^2/R^3 is the same for all planets

$$\mu \ddot{r} - \frac{l^2}{\mu r^3} + \frac{dV}{dr} = 0, \quad V = -\frac{\alpha}{r}, \quad \alpha > 0;$$



$$r = r(t), \quad \varphi = \varphi(t) \rightarrow r(\varphi(t))$$

$$\frac{d}{dt} = \dot{\varphi} \frac{d}{d\varphi} = \frac{l}{\mu r^2} \frac{d}{d\varphi};$$

$$\frac{d^2}{dt^2} = \frac{l^2}{\mu^2 r^2} \frac{d}{d\varphi} \left(\frac{1}{r^2} \frac{d}{d\varphi} \right)$$

$$u = \frac{1}{r};$$

$$\frac{dV}{dr} \equiv \frac{\alpha}{r^2} = \alpha u^2$$

$$\frac{d^2}{dt^2} \left(\frac{1}{u} \right) + \dots$$

$$\mu \frac{l^2 u^2}{\mu^2} \frac{d}{d\varphi} \left(u^2 \underbrace{\frac{d}{d\varphi} \frac{1}{u}}_{= -\frac{1}{u^2} \frac{du}{d\varphi}} \right) - \frac{l^2}{\mu} u^3 + \alpha u^2 = 0$$

multiply by $\frac{\mu}{l^2 u^2}$:

$$-\frac{d^2 u}{d\varphi^2} - u + \frac{\alpha \mu}{l^2} = 0;$$

$$\frac{d^2 u}{d\varphi^2} + u = \frac{\alpha \mu}{l^2}$$

ODE of harmonic oscillator

$$u \equiv \frac{1}{r} = \frac{\alpha \mu}{l^2} [\varepsilon \cos(\varphi - \varphi_0) + 1]$$

ε (called the **eccentricity**) and φ_0 are constants of integration

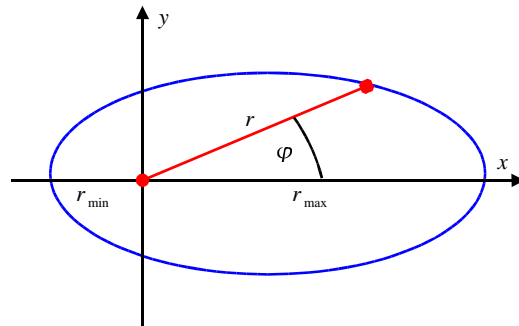
If $\varepsilon = 0 \Rightarrow$ orbit is a closed circle, $\varphi_0 = \pi$

$$\frac{1}{r} = \frac{\alpha \mu}{l^2} [1 - \varepsilon \cos \varphi]$$

$$0 < \varepsilon < 1$$

$$\varphi = \pi : r(\pi) = r_{\min} = \frac{l^2}{\alpha \mu (1 + \varepsilon)} \text{ perihelion}$$

$$\varphi = 0 : r(0) = r_{\max} = \frac{l^2}{\alpha \mu (1 - \varepsilon)} \text{ aphelion}$$



$$\frac{(x - a\varepsilon)^2}{a^2} + \frac{y^2}{b^2} = 1; \quad a = \frac{p}{1 - \varepsilon^2}, \quad b = \frac{p}{\sqrt{1 - \varepsilon^2}}, \quad p = \frac{l^2}{\alpha \mu};$$

$$r = r_{\min} : v \perp \text{position vector to the sun} \Rightarrow l = r_{\min} \mu v$$

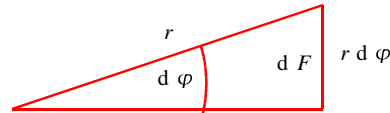
$$T = \frac{1}{2} \mu v^2 = \frac{1}{2} \mu \frac{l^2}{r_{\min}^2 \mu^2} = \frac{\mu \alpha^2 (\varepsilon + 1)^2}{2 l^2};$$

$$V = -\frac{\alpha}{r_{\min}}, \quad E = T + V = \frac{\mu \alpha^2 (\varepsilon + 1)^2}{2 l} - \frac{\alpha^2 \mu (1 + \varepsilon)^2}{l^2 \cdot 2} = \frac{\mu \alpha^2 (\varepsilon^2 - 1)}{2 l^2}; \quad \varepsilon = \sqrt{1 + \frac{2 E l^2}{\mu \alpha^2}};$$

If $\varepsilon < 1$ ($E < 0$) \Rightarrow closed orbit

If $\varepsilon \geq 1$ ($E > 0$) \Rightarrow open orbit, hyperbolic ($\varepsilon > 1$) or parabolic ($\varepsilon = 1$)

$$(K2): \quad \mu r^2 \dot{\varphi} = l = \text{const}$$



$$\frac{1}{2} r^2 d\varphi = dF;$$

$$\frac{1}{2} r^2 \dot{\varphi} = \dot{F} = const;$$

3.4 The Tangent Bundle TQ

Lagrange's equations are 2nd-order ODE on the configuration manifold Q .

Velocity phase manifold TQ .

Consider 2 particles move on the 2-D surface of a sphere: S^2

The velocity vector of each particle is tangent to the sphere:

$$\vec{v} \in \{ \text{tangent planes of all points } \in S^2 \}$$

The difference between the velocity vectors (at two different points) does not lie in either tangent plane.

The Lagrangian $L(q, \dot{q}, t); q \equiv \{q^\alpha | \alpha = 1, \dots, n = 3N - K\}$:

L depends on a larger manifold that is called (TQ) **velocity phase manifold**.

$$\dim(TQ) = 2n \quad q, \dot{q}$$

Tangent bundle or **tangent manifold** of Q .

The space TQ is obtained from Q by adjoining to each point $q \in Q$ the vector space, called the tangent space $T_q Q$, of all possible velocities at q , which are all tangent to Q at this point.

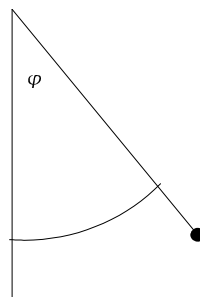
TQ is made up of Q plus all the $T_q Q$ for $q \in Q$.

Each point in TQ is $(q, \dot{q}) = \{(q^\alpha, \dot{q}^\alpha), \alpha = 1, \dots, n\}$ analogous to (x, v)

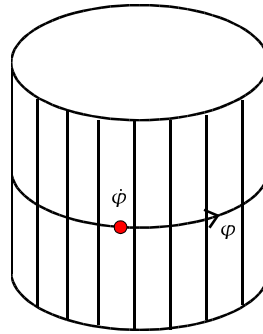
Through each point $(q, \dot{q}) \in TQ$ passes just one solution of the EM, one phase trajectory.

Therefore phase portraits can be constructed in TQ .

Example: Plan pendulum



$$Q = S^1 = \{ \varphi | 0 \leq \varphi \leq 2\pi \}; \quad \dot{\varphi} \in (-\infty, \infty)$$



$T S'$ is a cylinder to each $\varphi \in S'$, we attach an infinite line. The line attached to φ is $T_\varphi S'$ and is called the **fiber above** φ .

On $T Q$, the Lagrange's equations are a set of *first-order ODEs* for the $q^\alpha(t)$ and the $\dot{q}^\alpha(t)$.

$$n \text{ equations: } H(q, \dot{q}, t) \frac{d}{dt}(\dot{q}) = G(q, \dot{q}, t)$$

$$n \text{ equations: } \dot{q} = \frac{d}{dt}(q)$$

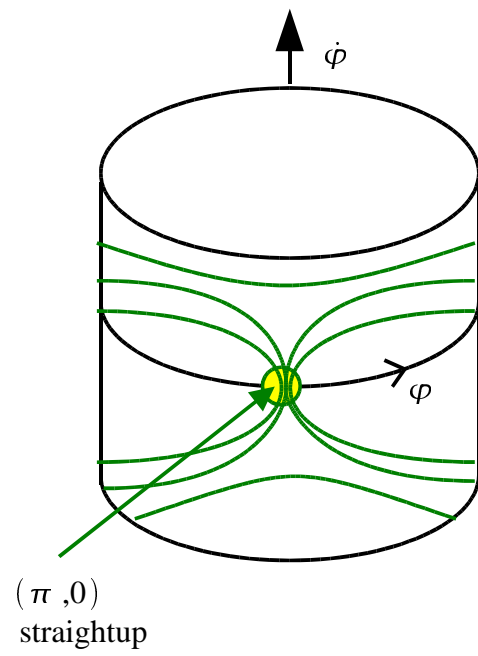
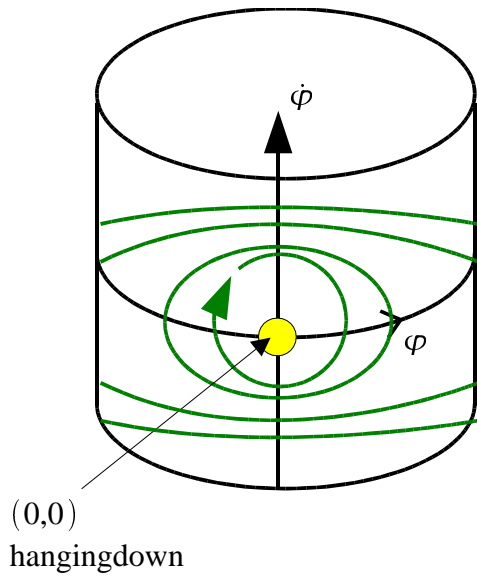
$\Rightarrow 2n$ equations for $2n$ unknowns

The initial conditions for these $2n$ 1st-order ODEs are the $2n$ initial values

$$(q_0, \dot{q}_0) \equiv \{q^\alpha(0), \dot{q}^\alpha(0)\}.$$

Thus, given the initial point in $T Q$, the rest of the trajectory is uniquely determined analytically by the $E_0 M$ or graphically by the phase portraits.

Example: Planependulum, $E = \frac{1}{2} m l^2 \dot{\varphi}^2 - m g h \cos \varphi = \text{const}$



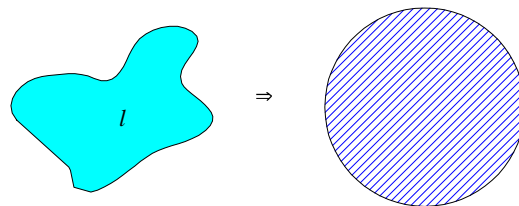
4. Topics in Lagrangian Dynamics

4.1 The Variational Principle and Lagrange's Equations

The Action

Examples of variational problems:

A. Given a fence of a fixed length. What shape provides the largest area it can surround? Answer: Circle!

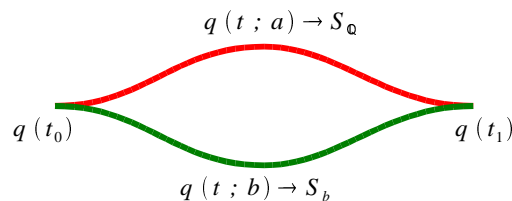


B. Optimization: How to choose some parameters in order to make some function or value an extremum?

Show: a dynamical system moves so as to minimize the action

$$S \equiv \int_{t_0}^{t_1} L(q, \dot{q}, t) dt$$

trajectory $q(t)$: S is a functional of $q(t)$, depends on $q(t)$ and all of $t \in [t_0, t_1]$



$S[q(t)] \stackrel{!}{=} \text{Minimum}$, domain = functionspace

Theorem (Hamilton's variational principle): The physical trajectory is the one for which S is a minimum.

Families of trajectories starting at $q(t_0)$ and ending at $q(t_1)$: $q(t; \varepsilon)$
 $\varepsilon = 0$: $S = \text{Minimum}$

$$\left. \frac{dS}{d\varepsilon} \right|_{\varepsilon=0} = \left[\frac{d}{d\varepsilon} \int_{t_0}^{t_1} L(q, \dot{q}, t) dt \right]_{\varepsilon=0} = 0$$

$$\left. \frac{d}{d\varepsilon} \right|_{\varepsilon=0} \equiv \delta$$

$$\delta S = \delta \int_{t_0}^{t_1} L(q, \dot{q}, t) dt = 0;$$

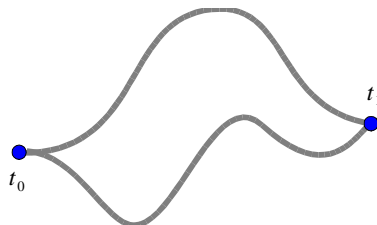
$$\delta L = \frac{\partial L}{\partial q^\alpha} \delta q^\alpha + \frac{\partial L}{\partial \dot{q}^\alpha} \delta \dot{q}^\alpha;$$

$$\frac{\partial L}{\partial \dot{q}^\alpha} \delta \dot{q}^\alpha = \frac{\partial L}{\partial \dot{q}^\alpha} \frac{d}{dt} (\delta q^\alpha) = \frac{d}{dt} \left[\frac{\partial L}{\partial \dot{q}^\alpha} \delta q^\alpha \right] - \left[\frac{d}{dt} \frac{\partial L}{\partial \dot{q}^\alpha} \right] \delta q^\alpha;$$

Order of d/dt and $d/d\varepsilon$ is arbitrary.

$$\delta L = \left[\frac{\partial L}{\partial q^\alpha} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}^\alpha} \right) \right] \delta q^\alpha + \frac{d}{dt} \left[\frac{\partial L}{\partial \dot{q}^\alpha} \delta q^\alpha \right]$$

$$0 = \delta S = \int_{t_0}^{t_1} \left[\frac{\partial L}{\partial q^\alpha} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}^\alpha} \right) \right] \delta q^\alpha dt + \underbrace{\int_{t_0}^{t_1} \frac{d}{dt} \left[\frac{\partial L}{\partial \dot{q}^\alpha} \delta q^\alpha \right] dt}_{\left. \frac{\partial L}{\partial \dot{q}^\alpha} \delta q^\alpha \right|_{t_0}^{t_1}} = 0$$



$$\int_{t_0}^{t_1} [\dots] \delta q^\alpha dt = 0$$

applies to any ε -family of trajectories

δq^α are arbitrary (vanish at endpoints)

$$\Rightarrow \frac{\partial L}{\partial q^\alpha} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}^\alpha} \right) = 0.$$

$$\int_{t_0}^{t_1} f_\alpha h_\alpha dt = (f, h)$$

$f, h \in F$ vector space with components $\{f_\alpha\}, \{h_\alpha\}$

If $(\Lambda, \delta q) = 0$ for arbitrary $\delta q \in F \Rightarrow \Lambda = 0$ ($\Lambda \perp \delta q$)

$$\Lambda_\alpha = \frac{\partial L}{\partial q^\alpha} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}^\alpha} \right)$$

Inclusion of constants :

Given: $\mathbb{Q}, L \in T\mathbb{Q}; \dim(T\mathbb{Q}) = 2n$

Wish to add additional constraints, may be holonomic or nonholonomic

$$f_j(q, \dot{q}, t) = 0 \quad j = 1, \dots, K (*)$$

where $K < n$ are the additional constraints.

Variational method: We now require that the **comparison paths** satisfy the new constraints.

Now: $\delta q \in F \left(\delta q_\alpha \equiv \frac{\partial q^\alpha}{\partial \varepsilon} \right)$ are not arbitrary but are restricted by (*)

$$\frac{\partial f_j}{\partial \varepsilon} \equiv \frac{\partial f_j}{\partial q^\alpha} \frac{\partial q^\alpha}{\partial \varepsilon} + \frac{\partial f_j}{\partial \dot{q}^\alpha} \frac{\partial \dot{q}^\alpha}{\partial \varepsilon} = 0$$

Multiply each of these K equations by an arbitrary sufficiently well behaved function $\lambda_j(t)$:

$$\int_{t_0}^{t_1} \sum_{j=1}^K \left[\lambda_j \frac{\partial f_j}{\partial q^\alpha} \frac{\partial q^\alpha}{\partial \varepsilon} + \lambda_j \frac{\partial f_j}{\partial \dot{q}^\alpha} \frac{\partial \dot{q}^\alpha}{\partial \varepsilon} \right] dt = 0$$

Use a trick as before to convert

$$\frac{\partial f}{\partial \dot{q}^\alpha} \frac{d}{dt} \left[\frac{\partial q^\alpha}{\partial \varepsilon} \right] \rightarrow \frac{d}{dt} \left(\frac{\partial f}{\partial \dot{q}^\alpha} \frac{\partial q^\alpha}{\partial \varepsilon} \right) - \dots \delta q^\alpha$$

$$\int_{t_0}^{t_1} \sum_j \left[\lambda_j \frac{\partial f_j}{\partial q^\alpha} - \frac{d}{dt} \left(\lambda_j \frac{\partial f_j}{\partial \dot{q}^\alpha} \right) \right] \frac{\partial q^\alpha}{\partial \varepsilon} dt = \left(\sum_j \Lambda_j, \delta q \right) = 0;$$

„allowed“ δq -vectors that satisfy $f_j = 0$.

Not that we still have $(\Lambda, \delta q) = 0$, $\Lambda \perp \delta q$, $\delta q \perp \sum_j \Lambda_j \Rightarrow$

$$\frac{d}{dt} \frac{\partial}{\partial \dot{q}^\alpha} \left(L + \sum_{j=1}^K \lambda_j f_j \right) - \frac{\partial}{\partial q^\alpha} \left(L + \sum_{j=1}^K \lambda_j f_j \right) = 0$$

λ_j are called **Lagrangemultipliers**

$$\tilde{L} = L + \sum_j \lambda_j f_j$$

If constraints are *holonomic*:

$$\frac{d}{dt} \frac{\partial L}{\partial \dot{q}^\alpha} - \frac{\partial L}{\partial q^\alpha} - \sum_j \lambda_j \frac{\partial f_j}{\partial q^\alpha} = 0 \quad \alpha = 1, \dots, n$$

$$f_j(q, t) = 0 \quad j = 1, \dots, K$$

$$\Rightarrow (q^\alpha, \lambda_j)$$

For *nonholonomic* constraints:

If constraints depend linearly on general velocities, use a trick:

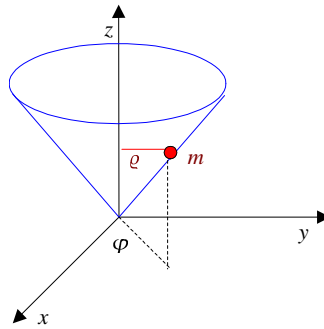
Assume $f_j = f_j(q) = 0$ are holonomic

\Rightarrow then we define *new constraints*

$$g_j \equiv \frac{df_j}{dt} = \frac{\partial f_j}{\partial q^\alpha} \dot{q}^\alpha = 0$$

$$\frac{d}{dt} \frac{\partial L}{\partial \dot{q}^\alpha} - \frac{\partial L}{\partial q^\alpha} - \sum_j \lambda_j \frac{\partial g_j}{\partial \dot{q}^\alpha} = 0$$

Example: A particle of mass m that moves under the influence of gravity on the inner surface of a cone $\sqrt{x^2 + y^2} = a z$ which is assumed to be frictionless.



$$V = m g z$$

$$L = \frac{1}{2} m (\dot{\rho}^2 + \rho^2 \dot{\phi}^2 + \dot{z}^2) - m g z$$

Additional constraints: $f = \rho - a z = 0 \quad (K = 1)$

$$(\rho, \phi, z) \rightarrow \frac{\partial f}{\partial \rho}, \frac{\partial f}{\partial \phi}, \frac{\partial f}{\partial z}$$

$$(1) \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\rho}} \right) - \frac{\partial L}{\partial \rho} = \lambda \Rightarrow m (\ddot{\rho} - \rho \dot{\phi}^2) = \lambda$$

$$(2) \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\phi}} \right) - \frac{\partial L}{\partial \phi} = 0 \Rightarrow m \frac{d}{dt} (\rho^2 \dot{\phi}) = 0 \Rightarrow m \rho^2 \dot{\phi} = l$$

$$(3) \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{z}} \right) - \frac{\partial L}{\partial z} = -\lambda a \Rightarrow m \ddot{z} = -m g - \lambda a$$

Inserting (2) into (1) and setting $a \ddot{z} = \ddot{\rho}$

$$\Rightarrow \lambda(t) = \frac{1}{1 + a^2} \left(-m g a - \frac{l^2}{m \rho^3} \right)$$

$$\ddot{\rho} = \frac{1}{2} \left(\frac{l}{m} \right)^2 \frac{1}{\rho^3} - \frac{g}{2}$$

$$\dot{\phi} = \frac{l}{m \rho^2}$$

$$z = \rho$$

4.2 Molecular dynamics

$$V(r_{ij}) = 4 \varepsilon \left[\left(\frac{\sigma}{r_{ij}} \right)^{12} - \left(\frac{\sigma}{r_{ij}} \right)^{-6} \right] \quad r_{ij} \leq r_c$$

first fraction: resistance to compression, repulsion at close range provided by closed inner shells of atoms

second fraction: attraction leading to binding

Liquid inert gas (argon) :

Van-der-Waals attraction

$r_{ij} = |\vec{r}_i - \vec{r}_j|$, ϵ governs the strength of interaction, σ length scale

$$\vec{F}_{ij} = \left(\frac{48 \epsilon}{\sigma^2} \right) \left[\left(\frac{\sigma}{r_{ij}} \right)^{14} - \frac{1}{2} \left(\frac{\sigma}{r_{ij}} \right)^8 \right] \vec{r}_{ij} \Rightarrow$$

$$m \ddot{\vec{r}}_i = \sum_{\substack{j=1 \\ (j \neq i)}} \vec{F}_{ij} \equiv \vec{F}_i$$

Kinetic energy per atom is

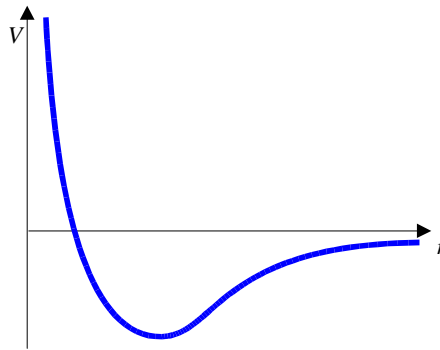
$$\frac{K}{N} = \frac{m}{2N} \sum_{i=1}^N v_i^2$$

Macroscopic temperature of an ensemble of particles:

$$\frac{3}{2} k_B T = \frac{m}{2N} \sum_{i=1}^N v_i^2$$

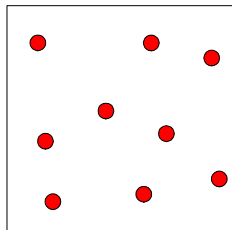
$k_B = 1.38065 \cdot 10^{-23} \text{ J K}^{-1}$ **Boltzmann constant**

Lennard-Jones, Los Alamos National Laboratories



Boundary Conditions :

Homogenous bulk systems: solids, liquids, gases in container. $N \sim 10^{29} \text{ m}^{-3}$, Computer:
 $N < 10^7$ atoms .



Number of atoms near walls:

$$\sim N^{\frac{2}{3}} \sim 10^{19} \frac{1}{\text{m}^2}$$

$\Rightarrow 1 : 10^{10}$ atoms

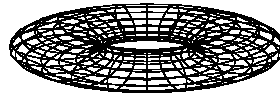
Simulation: $N \sim 1000$:roughly $N \sim 500$ lie close to walls!

Periodic boundary condition

1-D:

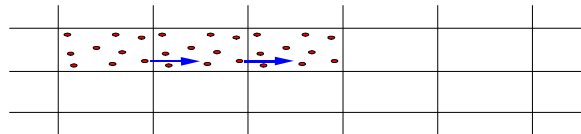


2-D: Torus



>3-D: n-dimensional Torus

Infinite space-filling array of identical copies of the simulation region:



2 consequences :

- Atom leaves to the right \Rightarrow reenter to the left
- Atoms lying within r_c of a boundary interact with atoms in an adjacent copy of the system \Rightarrow **wrap around effect**

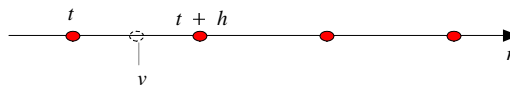
Integration:

- Runge-Kutta Method
- Leapfrog method („Bockspringer“)

$h = \Delta t$ timestep

$$v_{xi} \left(t + \frac{h}{2} \right) = v_{xi} \left(t - \frac{h}{2} \right) + h a_{xi} (t);$$

$$r_{xi} (t + h) = r_{xi} (t) + h v_{xi} \left(t + \frac{h}{2} \right)$$



Errors:

$O(h^4)$ for r

$O(h^2)$ for v

Typical timesteps for atoms: $1 \text{ fs} = 10^{-15} \text{ s}$

Constraint method for constant temperature

Initialize: random positions \vec{r} , random velocities \vec{v} such that:

$$\sum v_i^2 \stackrel{!}{=} \text{given temperature}$$

$$\frac{1}{2} m \sum_{i=1}^N \dot{\vec{r}}_i^2 = \alpha T = \text{const}$$

as constraint.

$$\ddot{\vec{r}}_i = \frac{1}{m} \vec{F}_i + \lambda \dot{\vec{r}}_i; \quad \text{multiply by } \dot{\vec{r}}_i$$

$$\dot{T} = 0 \Rightarrow \sum_i \dot{\vec{r}}_i \cdot \ddot{\vec{r}}_i = 0;$$

$$\Rightarrow \lambda = - \frac{\sum_i \dot{\vec{r}}_i \cdot \vec{F}_i}{m \sum_i \dot{\vec{r}}_i^2}$$

Modify the leapfrog velocity equation:

$$\vec{v}_i \left(t + \frac{h}{2} \right) = (1 + \lambda h) \vec{v}_i \left(t - \frac{h}{2} \right) + h \left(1 + \frac{\lambda h}{2} \right) \vec{F}_i(t)$$

where

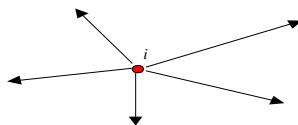
$$\lambda = - \frac{\sum_i \vec{v}_i(t) \cdot \vec{F}_i(t)}{\sum_i v_i^2(t)}$$

and

$$\vec{v}_i(t) = \vec{v}_i \left(t - \frac{h}{2} \right) + \frac{h}{2} \vec{F}_i(t)$$

Interaction computations: Cell subdivision

Force felt by 1 particle:

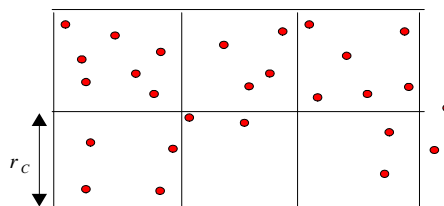


effort $\propto O(N^2)$

Concept of cell subdivision:

Divides simulation region into a lattice of small cells with cell edges slightly exceed

r_c in length.



Atoms are assigned to cells on the basis of their current positions \Rightarrow only atoms in adjacent cells

interact.

Because of symmetry: only half the neighboring cells need to be considered.

Data organization: linked lists

Economize storage: linked list associates a pointer with each particle that points to the next until a pointer value 0 is encountered, terminating the list. A separate list is required for each cell.

4.3 Cyclic coordinates

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}^\alpha} \right) = \frac{\partial L}{\partial q^\alpha};$$

q^β does not appear in L

$$\Rightarrow \frac{\partial L}{\partial q^\alpha} = 0 \Rightarrow \frac{\partial L}{\partial \dot{q}^\alpha} = \text{const of motion}$$

$$P_\beta (q, \dot{q}, t) \equiv \frac{\partial L}{\partial \dot{q}^\beta}$$

Generalized momentum conjugate to q^β :

Such coordinate q^β is called **cyclic** or **ignorable coordinate**.

If initial phase point lies on any submanifold whose equation is of the form $P_\beta = C$, the motion stays on that submanifold.

Example 1:

$$L = \frac{1}{2} \mu (\dot{r}^2 + r^2 \dot{\phi}^2) - V(r)$$

$$\Rightarrow P_\phi \equiv \frac{\partial L}{\partial \dot{\phi}} = \mu r^2 \dot{\phi} = \text{conserved} = \tilde{C}$$

Example 2: A free particle in cartesian coordinates

$$L = \frac{1}{2} m (\dot{x}^2 + \dot{y}^2 + \dot{z}^2)$$

$$\Rightarrow P_x \equiv \frac{\partial L}{\partial \dot{x}} = m \dot{x} = \text{conserved}$$

Note: If q^λ is ignorable, then $\partial L / \partial q^\lambda = 0$, which means that L does not change as q^λ varies, or L is invariant under translation in the q^λ direction in $T\mathbb{Q}$.

Example 3:

$$L = \frac{1}{2} m (\dot{x}^2 + \dot{y}^2 + \dot{z}^2) - m g z.$$

4.4 Dissipative Forces in the Lagrangian Formalism

$$\sum_{i=0}^N (m_i \ddot{\vec{x}}_i - \vec{F}_i) \frac{\partial \vec{x}_i}{\partial q^\alpha} = 0 \quad \alpha = 1, \dots, n$$

$$\vec{F}_i = -\vec{\nabla} V(\vec{x}_1, \dots, \vec{x}_N)$$

$$\sum_{i=1}^N \vec{F}_i \frac{\partial \vec{x}_i}{\partial q^\alpha} = -\sum_i \vec{\nabla}_i V \frac{\partial \vec{x}_i}{\partial q^\alpha} = -\frac{\partial V}{\partial q^\alpha}$$

$$\text{Now: } \vec{F}_i = \vec{F}_{P_i} + \vec{F}_{D_i}$$

where $\text{curl}_i \vec{F}_{P_i} = 0$ but $\text{curl}_i \vec{F}_{D_i} \neq 0$

$$\sum_i \vec{F}_{D_i} \frac{\partial \vec{x}_i}{\partial q^\alpha} \equiv D_\alpha$$

$$\sum_i \vec{F}_i \frac{\partial \vec{x}_i}{\partial q^\alpha} = -\frac{\partial V}{\partial q^\alpha} + D_\alpha$$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}^\alpha} \right) - \frac{\partial L}{\partial q^\alpha} = D_\alpha$$

$$L = T - V$$

$$\vec{F}_{D_i} = -b_i \vec{v}_i \quad b_i > 0$$

These forces do negative work on the particle as it moves \Rightarrow leads to energy loss. Forces are called **dissipative**.

$$D_\alpha = -\sum_i b_i \vec{v}_i \frac{\partial \vec{x}_i}{\partial q^\alpha} = -\sum_i b_i \vec{v}_i \frac{\partial \vec{v}_i}{\partial \dot{q}^\alpha} = -\frac{\partial \tilde{F}}{\partial \dot{q}^\alpha}, \quad \tilde{F} = \sum_{i=1}^N \frac{1}{2} b_i v_i^2$$

Note: \vec{v}_i are the real velocities, \dot{q}^α are generalized velocities.
 \tilde{F} is called the **Rayleigh function**.

The rate of energy loss:

$$\begin{aligned} \frac{dE}{dt} &= \frac{d}{dt} \left(\dot{q}^\alpha \frac{\partial L}{\partial \dot{q}^\alpha} - L \right) = \ddot{q}^\alpha \frac{\partial L}{\partial \dot{q}^\alpha} + \dot{q}^\alpha \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}^\alpha} \right) - \frac{dL}{dt} \\ &= \dot{q}^\alpha \left(\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}^\alpha} \right) - \frac{\partial L}{\partial q^\alpha} \right) = -\dot{q}^\alpha \frac{\partial \tilde{F}}{\partial \dot{q}^\alpha} \end{aligned}$$

Cartesian coordinates:

$$-\sum_i \vec{v}_i \vec{F}_{D_i} = \text{Power loss} = \text{rate of energy loss}$$

Example: Equilibrium lattice constant of an inert gas crystal

The lattice constant of a simple cubic lattice. Crystal: periodic.

Equilibrium: Atoms at rest

$$E_{tot} = \frac{1}{2} \sum_j V(r_{ij});$$

$$r_{ij} = |\vec{r}_i - \vec{r}_j|$$

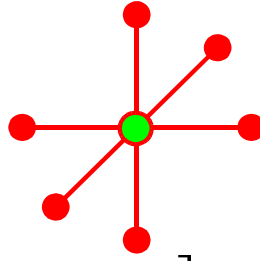
Atoms: denumerable set

$$\vec{r}_i = a (n \vec{e}_x + m \vec{e}_y + k \vec{e}_z) = a \vec{u}_{nmk} \quad n, m, k \in \mathbb{Z} \text{ (integers)}$$

a : lattice constant

$$\vec{r}_{ij} : (i, j) \rightarrow (i, \underbrace{j}_l)$$

$$E_{tot} = \frac{1}{2} \sum_{i,l} V(r_l) = \frac{1}{2} N \sum_l V(r_l)$$



$$E_{tot} = \frac{1}{2} N \cdot 4 \cdot \varepsilon \left[\sum_{n m k} \left(\frac{\sigma}{a u_{nmk}} \right)^{12} - \sum_{n m k} \left(\frac{\sigma}{a u_{nmk}} \right)^6 \right]$$

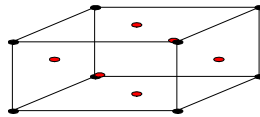
$$\sum_{n m k} ' u_{nmk}^{-12} = 6 \quad (\sum ' \text{ means: } n = m = k = 0 \text{ excluded})$$

$$\sum_{n m k} ' u_{nmk}^{-6} = 6$$

$$\frac{d E_{tot}}{d a} = 0 = -2 N \cdot \varepsilon \left[12 \cdot 6 \frac{\sigma^{12}}{a^{13}} - 6 \cdot 6 \frac{\sigma^6}{a^7} \right] \Rightarrow \frac{a}{\sigma} = 2^{\frac{1}{6}} = 1.12$$

Experimentally: all inert gas crystals have lattice constants where

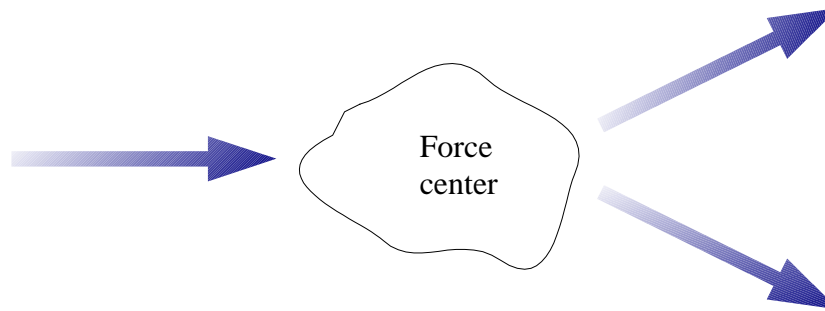
$a/r \approx 1.09$ (face centered cubic)



5.ScatteringandLinearOscillators

5.1Scattering

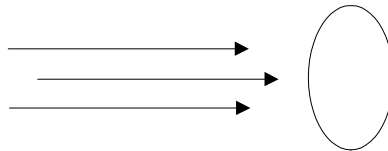
Consider a central-forced dynamical system that possesses unbounded orbits.



Angle between the distant incoming velocity vector and the distant outgoing one is the **scattering angle**.

Consider a beam of noninteracting particles incident on a stationary target consists of a collection of other particles.

The **flux density** or **intensity** I of beam = number of particles crossing a unit area perpendicular to the beam per unit time.



A = beam's cross-sectional area

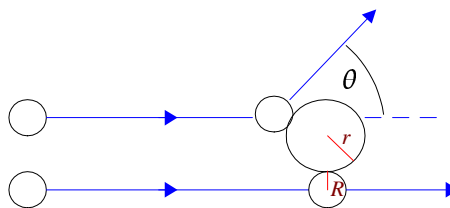
n = number of target particles per unit area = density of target particles

Assume: beam particles interact with target particles through a hard-sphere interaction

⇒ Cross-sectional area of this interaction is $\sigma = \pi (r + R)^2$ where

r = radius of target particle

R = radius of beam particle

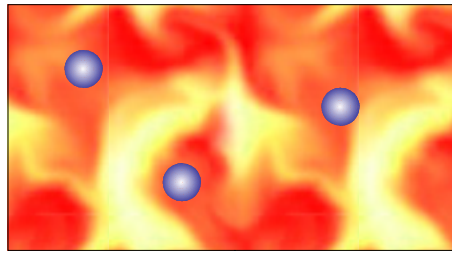


⇒ The total interaction cross section that the target particles present to the beam is

$$\Sigma = n A \sigma - N \sigma$$

N = number of target particles within the cross-sectional area of the beam

⇒ On the average, the number of collisions per unit time = $I \Sigma$



$$\sigma = \pi (r + R)^2$$

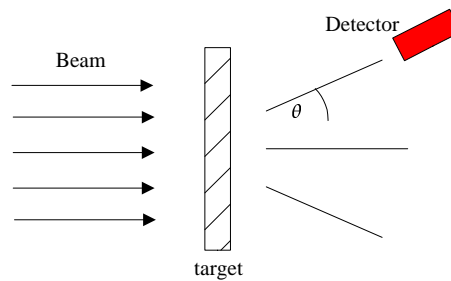
Scattering rate: number of particles scattered out of the beam per unit time =

$$S = I \sum = I N \sigma$$

For arbitrary interactions: total cross section σ_{tot} per particle:

$$\sigma = \frac{\text{out-flux}}{\text{in-flux per unit area}} \text{ [area]}$$

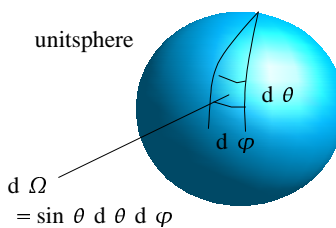
In experiment: place a detector at some distance from target



colatitude θ

azimuth φ

Detector subtends a small solid angle $d\Omega = \sin \theta d\theta d\varphi$

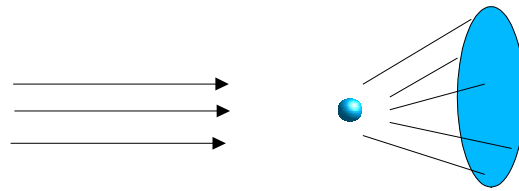


detects a number dS of particles, $dS = I N \sigma(\theta, \varphi) d\Omega$, where $\sigma(\theta, \varphi)$ is the **differential cross section** and

$$\sigma_{tot} = \int \sigma(\theta, \varphi) d\Omega.$$

Single target particle $N = 1$; central-force interaction. Let this target particle be in the center of the beam

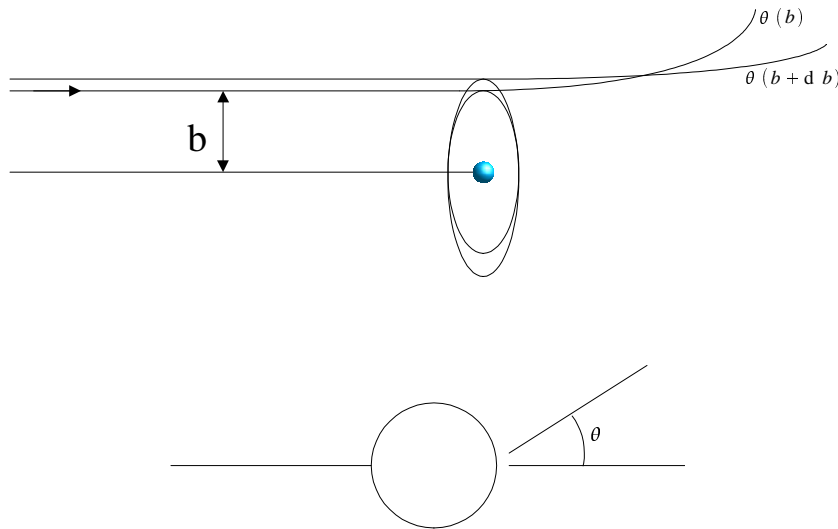
$$\Rightarrow \sigma = \sigma(\theta)$$



$$2 \pi \sigma (\theta) \sin \theta d \theta = \frac{d S}{I}$$

$d S$ = number of particles scattered into angles between θ and $\theta + d \theta$ for any φ .

Consider an incident particle aimed some distance b (called the **impact parameter**) from the target particle.



The part of the beam that lies in the ring of radius b and of width $d b$ gets scattered through angles θ to $\theta + d \theta$.

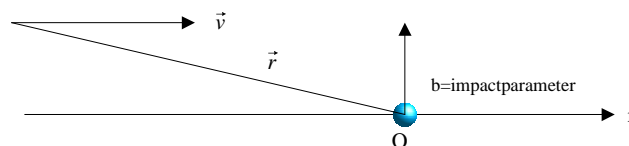
This ring has $2 \pi b d b$.

Number of particles scattered into $d \theta$ interval =

$$\underbrace{2 \pi b d b \cdot I}_A$$

$$2 \pi b (\theta) d b = -2 \pi \sigma (\theta) \sin \theta d \theta$$

b depends on initial conditions



$$l = \mu v b$$

At $r = -\infty$:

$$E = \frac{1}{2} \mu v^2$$

$$l = b \sqrt{2 \mu E}$$

Total energy of relative motion was

$$E = \frac{1}{2} \mu \dot{r}^2 + \frac{1}{2} \mu r^2 \dot{\varphi}^2 + V(r)$$

$$\frac{d}{dt} = \underbrace{\frac{l}{\mu r^2}}_{=\dot{\varphi}} \frac{d}{d\varphi}$$

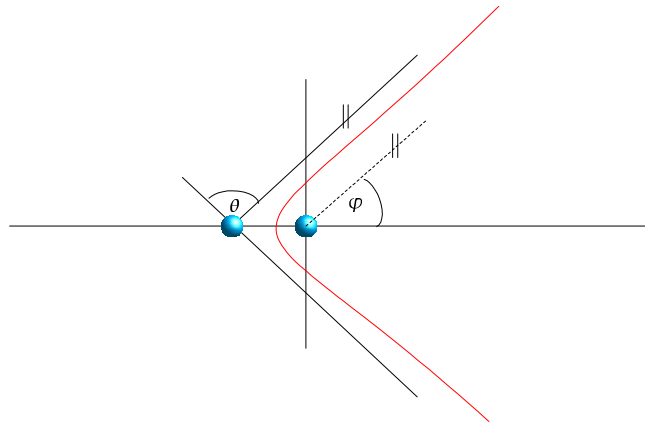
$$E = \frac{l^2}{2 \mu r^4} \left(\frac{dr}{d\varphi} \right)^2 + \frac{l^2}{2 \mu r^2} + V(r)$$

$$\frac{d\varphi}{dr} = \left(\frac{dr}{d\varphi} \right)^{-1}$$

⇒ integrate motion from r_0 to r

$$\varphi(r) = \sqrt{\frac{l^2}{2 \mu}} \int_{r_0}^r \frac{dr}{r^2 \sqrt{E - V(r) - \frac{l^2}{2 \mu r^2}}}$$

Angle $\varphi \leftrightarrow$ scattering angle θ



$$\theta = \pi - 2 \varphi$$

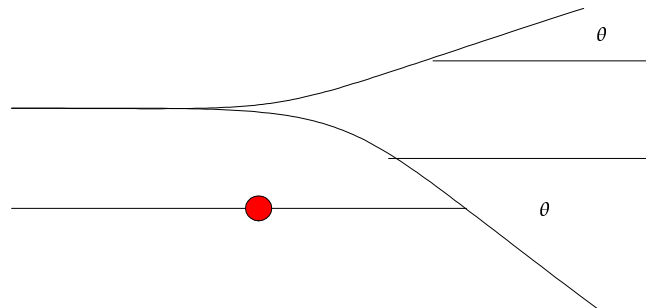
$$\theta = \pi - 2 b \int_{r_0}^{\infty} \frac{dr}{r \sqrt{r^2 \left[1 - \frac{V(r)}{E} \right] - b^2}}$$

where r_0 is the minimum radius = $\sqrt{\dots}$

Apply this recipe to the Coulomb force $V(r) = \pm \alpha / r$, beam particles of mass $m \Rightarrow$

Rutherford scattering cross section

$$\sigma(\theta) = \frac{\alpha^2}{4 m^2 v^2} \frac{1}{\sin^4 \frac{\theta}{2}}$$



$$\sigma_{tot}(\text{Coulomb}) = \int d\Omega \sigma(\theta) = \infty$$

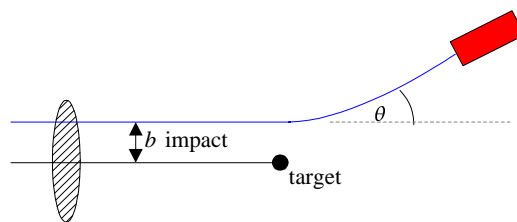
⇒ long-rangennatureofCoulombpotential

Realpotential:

$$\mp \frac{\alpha}{r} e^{-\lambda r}$$

screenedCoulombpotential

$$\sigma(\theta, \varphi) = \frac{d\sigma}{d\Omega} = \frac{\text{\#particlesscatteredinto } d\Omega \text{ per unittime}}{\text{\#particlesincomingperunittimeandunitsource}}$$



Differentialcrosssection(„differenziellerWirkungsquerschnitt“),solidangle(„Raumwinkel“)

5.2 Linear Oscillations

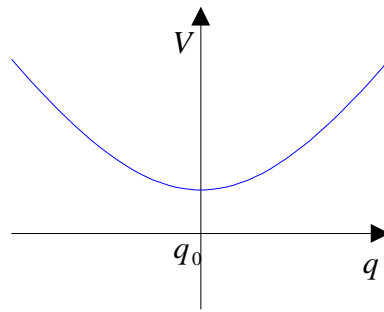
5.2.1 Linear Approximation, small vibrations

q_0 = stable equilibrium point of a Lagrangian system in one freedom

Potential energy is:

$$V(q) = V(q_0) + (q - q_0) V'(q_0) + \frac{1}{2} (q - q_0)^2 V''(q_0) + \dots \text{ (Taylor)}$$

$$V'(q_0) = 0$$



$$x \equiv q - q_0 \Rightarrow$$

$$L(x, \dot{x}) = \frac{1}{2} m \dot{x}^2 - \frac{1}{2} k x^2$$

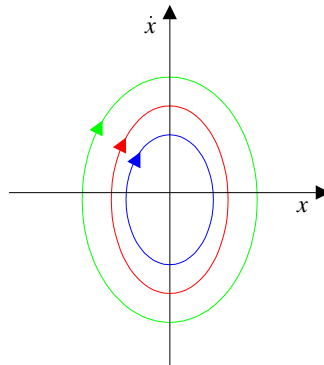
$$\Rightarrow \ddot{x} + \omega^2 x = 0, \quad \omega = \sqrt{\frac{k}{m}}$$

$k = V''(q_0)$ **force constant** or **effective spring constant**

$$x(t) = a \cos \omega t + b \sin \omega t = C \cos(\omega t + \delta) = \operatorname{Re}(\alpha e^{i\omega t}) = \alpha e^{i\omega t} + \alpha^* e^{-i\omega t}$$

$$E = \frac{1}{2} m \dot{x}^2 + \frac{1}{2} k x^2 = \frac{1}{2} m \underbrace{C^2 \omega^2}_{=k C^2} \sin^2(\omega t + \delta) + \frac{1}{2} k C^2 \cos^2(\omega t + \delta) = \frac{1}{2} k C^2 = \text{const}$$

$$\frac{\dot{x}^2}{\omega^2 C^2} + \frac{x^2}{C^2} = 1$$



Origin: $x = \dot{x} = 0$

$$L = \frac{1}{2} m_{\alpha\beta}(q) \dot{q}^\alpha \dot{q}^\beta - V(q)$$

$V(q)$ has minimum at same q_0 :

$$\left. \frac{\partial V}{\partial q^\beta} \right|_{q_0} = 0 \quad \forall \beta = 1, \dots, n$$

q_0 is stable equilibrium point

$$V(x) \approx \frac{1}{2} K_{\alpha\beta} x^\alpha x^\beta$$

$$K_{\alpha\beta} = \left. \frac{\partial^2 V}{\partial x^\alpha \partial x^\beta} \right|_{x=0}$$

$$x^\alpha = q^\alpha - q_0^\alpha$$

$x = 0$ is minimum $\Rightarrow K_{\alpha\beta}$ forms a positive matrix, i.e.

$$V(x) \equiv K_{\alpha\beta} x^\alpha x^\beta \geq 0 \quad \forall x \neq 0$$

\leftrightarrow is called **force constant matrix**

$$m_{\alpha\beta}(q) = M_{\alpha\beta} + R_{\alpha\beta\gamma} x^\gamma + \dots$$

$T > 0 \Rightarrow M_{\alpha\beta}$ is positive definite,

$$M_{\alpha\beta} \dot{x}^\alpha \dot{x}^\beta > 0 \quad \forall \dot{x} > 0$$

\Rightarrow to lowest order in x

$$L = \frac{1}{2} M_{\alpha\beta} \dot{x}^\alpha \dot{x}^\beta - \frac{1}{2} K_{\alpha\beta} x^\alpha x^\beta \Rightarrow$$

$$\ddot{x}^\alpha + \Lambda^\alpha_\beta x^\beta = 0$$

$$\Lambda^\alpha_\beta = M_{\alpha\gamma}^{-1} K_{\gamma\beta}$$

$$L = \frac{1}{2} (\dot{\vec{x}}, \overset{\leftrightarrow}{M} \dot{\vec{x}}) - \frac{1}{2} (\vec{x}, \overset{\leftrightarrow}{K} \vec{x})$$

Note: M^{-1} exists since M is positive definite.

Equations of n coupled oscillators:

$$L \in T_{q_0} \mathbb{Q}, \vec{x} = (x^\alpha) \text{ are directions in } T_{q_0} \mathbb{Q}, \text{ and } (\vec{x}, \vec{y}) = x_\alpha y_\alpha$$

$$\ddot{\vec{x}} + \overset{\leftrightarrow}{\Lambda} \vec{x} = 0$$

$$\overset{\leftrightarrow}{\Lambda} = \overset{\leftrightarrow}{M}^{-1} \overset{\leftrightarrow}{K}$$

Solutions are called **normal modes** \leftrightarrow Eigenvectors and eigenvalues of $\overset{\leftrightarrow}{\Lambda}$

$$\overset{\leftrightarrow}{\Lambda} \vec{x} = \lambda \vec{x}$$

$$\Rightarrow \ddot{\vec{x}} = -\lambda \vec{x} = -\omega^2 \vec{x}$$

Normal frequencies ω . The eigenvectors oscillate like independent one-freedom harmonic oscillators and thus point along the normal modes. The ω are square roots of the eigenvalues of

$$\overset{\leftrightarrow}{\Lambda}.$$

$$\omega \text{ real} \Rightarrow \lambda \geq 0$$

$$\lambda = 0: \ddot{\vec{x}} = 0 \Rightarrow \vec{x} = \vec{A} t + \vec{B} \text{ force free motion of the whole system}$$

Let \vec{a} be an eigenvector:

$$\overset{\leftrightarrow}{\Lambda} \vec{a} = \omega^2 \vec{a}$$

$$\Rightarrow \vec{x}(t) = \vec{a} (\alpha e^{i\omega t} + \alpha^* e^{-i\omega t}) = 2\vec{a} \{A \cos \omega t + B \sin \omega t\}$$

$$[A = \operatorname{Re} \alpha, B = -\operatorname{Im} \alpha]$$

$$\vec{x}(t) = \sum_{y=1}^n \vec{a}_y [\alpha_y e^{i\omega_y t} + \alpha_y^* e^{-i\omega_y t}]$$

$$\alpha = \operatorname{Re} \alpha + i \operatorname{Im} \alpha = \alpha_R + i \alpha_I;$$

$$(\alpha_R + i \alpha_I) (\cos \omega t + i \sin \omega t) + (\alpha_R - i \alpha_I) (\cos \omega t - i \sin \omega t) = 2 \alpha_R \cos \omega t - 2 \alpha_I \sin \omega t$$

Example: Idealized linear classical water molecule



Let equilibrium distance between neighboring atoms be b

$$x_2^0 - x_1^0 = b, x_3^0 - x_2^0 = b$$

$$V(x_1, x_2, x_3) = \frac{k}{2} [(x_2 - x_1 - b)^2 + (x_3 - x_2 - b)^2]$$

$$q_i = x_i - x_i^0$$

$$V(q_1, q_2, q_3) = \frac{k}{2} [(q_2 - q_1)^2 + (q_3 - q_2)^2]$$

$$T(\dot{x}_1, \dot{x}_2, \dot{x}_3) = \frac{m}{2} (\dot{x}_1^2 + \dot{x}_3^2) + \frac{M}{2} \dot{x}_2^2 = \frac{m}{2} (\dot{q}_1^2 + \dot{q}_3^2) + \frac{M}{2} \dot{q}_2^2$$

$$L(q, \dot{q}) = \frac{1}{2} \sum_{i,j=1}^3 [M_{ij} \dot{q}_i \dot{q}_j - K_{ij} q_i q_j]$$

$$\overleftrightarrow{M} = \begin{pmatrix} m & 0 & 0 \\ 0 & M & 0 \\ 0 & 0 & m \end{pmatrix}, \quad \overleftrightarrow{M}^{-1} = \begin{pmatrix} \frac{1}{m} & 0 & 0 \\ 0 & \frac{1}{M} & 0 \\ 0 & 0 & \frac{1}{m} \end{pmatrix}, \quad \overleftrightarrow{K} = k \begin{pmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{pmatrix}$$

$$V = \frac{k}{2} [2q_2^2 - q_2q_1 - q_1q_2 + q_1^2 + q_3^2 - q_3q_2 - q_2q_3] = \frac{k}{2} \sum_{i,j} K_{ij} q_i q_j$$

$$\overleftrightarrow{\Lambda} = \overleftrightarrow{M}^{-1} \overleftrightarrow{K} = k \begin{pmatrix} \frac{1}{m} & -\frac{1}{m} & 0 \\ -\frac{1}{M} & \frac{2}{M} & -\frac{1}{M} \\ 0 & -\frac{1}{m} & \frac{1}{m} \end{pmatrix}$$

$$\overleftrightarrow{\Lambda} \vec{q} = \omega^2 \vec{q} \Leftrightarrow (\overleftrightarrow{\Lambda} - \omega^2 \overleftrightarrow{E}) \vec{q} = 0$$

$$\det(\overset{\leftrightarrow}{\Lambda} - \omega^2 \overset{\leftrightarrow}{E}) = 0 = \begin{vmatrix} \frac{k}{m} - \omega^2 & -\frac{k}{m} & 0 \\ -\frac{k}{M} & \frac{2k}{M} - \omega^2 & -\frac{k}{M} \\ 0 & -\frac{k}{m} & \frac{k}{m} - \omega^2 \end{vmatrix} = \begin{pmatrix} \lambda \equiv \frac{k}{m} \\ \mu \equiv \frac{k}{M} \end{pmatrix}$$

$$= \begin{vmatrix} \lambda - \omega^2 & -\lambda & 0 \\ -\mu & 2\mu - \omega^2 & -\mu \\ 0 & -\lambda & \lambda - \omega^2 \end{vmatrix} = \lambda \begin{vmatrix} -\mu & -\mu \\ 0 & \lambda - \omega^2 \end{vmatrix} + (\lambda - \omega^2) \begin{vmatrix} 2\mu - \omega^2 & -\mu \\ -\lambda & \lambda - \omega^2 \end{vmatrix}$$

$$= -\lambda \mu (\lambda - \omega^2) + (\lambda - \omega^2) [(\lambda - \omega^2)(2\mu - \omega^2) - \lambda \mu]$$

$$= (\lambda - \omega^2) \underbrace{[(\lambda - \omega^2)(2\mu - \omega^2) - 2\lambda \mu]}_{= \omega^2(\omega^2 - 2\mu - \lambda)} (\lambda - \omega^2) \omega^2 (\omega^2 - 2\mu - \lambda) = 0$$

\Rightarrow Normalfrequencies ω_y

$$\omega_1 = \sqrt{\frac{k}{m}}, \omega_2 = \sqrt{k \left(\frac{1}{m} + \frac{2}{M} \right)}, \omega_3 = 0$$

$$(\Lambda - \omega_\lambda^2) \vec{q} = 0$$

$$\vec{q}_1 = \begin{pmatrix} 1 \\ 0 \\ -1 \end{pmatrix}, \vec{q}_2 = \begin{pmatrix} 1 \\ -2 \frac{m}{M} \\ 1 \end{pmatrix}, \vec{q}_3 = \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} \alpha$$

$$(q_{11} = 1)$$

$$\begin{pmatrix} q_1(t) \\ q_2(t) \\ q_3(t) \end{pmatrix} = \begin{pmatrix} 1 \\ 0 \\ -1 \end{pmatrix} \{ \alpha_1 e^{i\omega_1 t} + \alpha_1^* e^{-i\omega_1 t} \} + \begin{pmatrix} 1 \\ -2 \frac{m}{M} \\ 1 \end{pmatrix} \{ \alpha_2 e^{i\omega_2 t} + \alpha_2^* e^{-i\omega_2 t} \} + \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} (a + vt)$$

$$q_1(0) = -A, q_2(0) = A \frac{m}{M}, q_3(0) = 0$$

$$\dot{q}_y(0) = 0 \quad \forall y$$

$$\begin{pmatrix} q_1(t) \\ q_2(t) \\ q_3(t) \end{pmatrix} = \frac{1}{2} A \begin{pmatrix} \cos \omega_1 t + \cos \omega_2 t \\ -2 \frac{m}{M} \cos \omega_2 t \\ -\cos \omega_1 t + \cos \omega_2 t \end{pmatrix}$$

$$L = \frac{1}{2} \left(\dot{\vec{x}}, \overset{\leftrightarrow}{M} \dot{\vec{x}} \right) - \frac{1}{2} \left(\vec{x}, \overset{\leftrightarrow}{K} \vec{x} \right)$$

$$\ddot{\vec{x}} = +\overset{\leftrightarrow}{\Lambda} \vec{x} = 0$$

$$\overset{\leftrightarrow}{\Lambda} = \overset{\leftrightarrow}{M}^{-1} \overset{\leftrightarrow}{K}$$

$$\overset{\leftrightarrow}{\Lambda} \vec{x} = \lambda \vec{x} \quad ; \quad \lambda \equiv \omega^2$$

- 1) Given an arbitrary square matrix $A_{n \times n}$, $a_{ij} \in \mathbb{R}$. Then A possesses exactly n eigenvalues $\lambda_i \in \mathbb{C}$. If $\lambda_i \neq \lambda_j$, $\forall i, j$, then there exist exactly n linearly independent eigenvectors.
- 2) Given a real symmetric matrix. All eigenvalues are real. If $\lambda_i \neq \lambda_j$, $\forall i, j$, the eigenvectors are orthogonal to each other. If an eigenvalue is p -fold degenerated, there exists p linearly independent eigenvectors that may be orthogonalized (e.g. by the Gram-Schmid-Procedure). \Rightarrow

Orthogonale eigenvectors

- 3) Given A, B . A, B are real symmetric matrices ($n \times n$). If $AB \neq BA \Rightarrow AB$ is not symmetric. Therefore, its eigenvectors are not orthogonal even though $\lambda_i \neq \lambda_j \quad \forall i, j$

$$\overset{\leftrightarrow}{A} \overset{\leftrightarrow}{x} = \omega^2 \overset{\leftrightarrow}{x}$$

$$A = \underbrace{\begin{pmatrix} \frac{1}{m} & 0 & 0 \\ 0 & \frac{1}{M} & 0 \\ 0 & 0 & \frac{1}{m} \end{pmatrix}}_{M^{-1}} \underbrace{\begin{pmatrix} \frac{k}{m} & -\frac{k}{m} & 0 \\ -\frac{k}{M} & \frac{2k}{M} & -\frac{k}{M} \\ 0 & -\frac{k}{m} & \frac{k}{m} \end{pmatrix}}_K$$

$$\omega_1 = \sqrt{\frac{k}{m}}, \quad \omega_2 = \sqrt{k \left(\frac{1}{m} + \frac{2}{M} \right)}, \quad \omega_3 = 0$$

$$\vec{q}_1 = c_1 \begin{pmatrix} 1 \\ 0 \\ -1 \end{pmatrix}, \quad \vec{q}_2 = c_2 \begin{pmatrix} 1 \\ -2 \frac{m}{M} \\ 1 \end{pmatrix}, \quad \vec{q}_3 = c_3 \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$$

$$\overset{\leftrightarrow}{M}^{-1} \overset{\leftrightarrow}{K} \overset{\leftrightarrow}{x} = \omega^2 \overset{\leftrightarrow}{x}$$

$$\overset{\leftrightarrow}{M}^{-\frac{1}{2}} \overset{\leftrightarrow}{K} \overset{\leftrightarrow}{x} = \omega^2 \overset{\leftrightarrow}{M}^{-\frac{1}{2}} \overset{\leftrightarrow}{x}$$

$$\overset{\leftrightarrow}{M}^{-\frac{1}{2}} \overset{\leftrightarrow}{K} \overset{\leftrightarrow}{M}^{-\frac{1}{2}} \overset{\leftrightarrow}{M}^{\frac{1}{2}} \overset{\leftrightarrow}{x} = \omega^2 \overset{\leftrightarrow}{M}^{\frac{1}{2}} \overset{\leftrightarrow}{x}$$

$$\overset{\leftrightarrow}{M}^{-\frac{1}{2}} \overset{\leftrightarrow}{K} \overset{\leftrightarrow}{M}^{-\frac{1}{2}} \overset{\leftrightarrow}{y} = \omega^2 \overset{\leftrightarrow}{y}$$

$$\overset{\leftrightarrow}{M}^{-\frac{1}{2}} \overset{\leftrightarrow}{K} \overset{\leftrightarrow}{M}^{-\frac{1}{2}} = \begin{pmatrix} \frac{k}{m} & -\frac{k}{\sqrt{m} M} & 0 \\ -\frac{k}{\sqrt{m} M} & \frac{2k}{M} & -\frac{k}{\sqrt{m} M} \\ 0 & -\frac{k}{\sqrt{m} M} & \frac{k}{m} \end{pmatrix}$$

$$\vec{y}_1 = c_1 \begin{pmatrix} 1 \\ 0 \\ -1 \end{pmatrix}, \quad \vec{y}_2 = c_2 \begin{pmatrix} 1 \\ -2 \sqrt{\frac{m}{M}} \\ 1 \end{pmatrix}, \quad \vec{y}_3 = c_3 \begin{pmatrix} 1 \\ \sqrt{\frac{M}{m}} \\ 1 \end{pmatrix}$$

5.2.2 Forced and Damped Oscillations

One-freedom case: undamped harmonic oscillator driven by an additional external time-dependent force $F(t)$.

If the force depends only on time, it can easily be fit into the Lagrangian formalism. The time-dependent Lagrangian

$$L'(q, \dot{q}, t) = L(q, \dot{q}) + q F(t) \quad (L' \text{ does not mean „derivative“})$$

$$m \ddot{q} = -\frac{\partial V}{\partial q} + F(t)$$

Oscillator:

$$L = \frac{1}{2} m \dot{q}^2 - \frac{1}{2} k q^2 + q F(t)$$

$$\ddot{q} + \omega_0^2 q = f(t); (*)$$

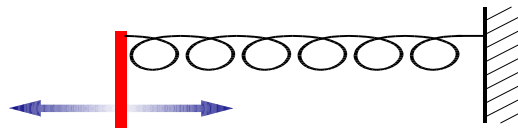
$$f(t) = \frac{F(t)}{m}, \quad \omega_0 = \sqrt{\frac{k}{m}}$$

forced or driven oscillator

Assume: Driving force $F(t) = F_0 \cos \Omega t$

ω : angular velocity of the oscillator

Ω : angular velocity of the driving force



A particular solution has the form

$$C \cos(\Omega t + \gamma)$$

$$(*) \Rightarrow \gamma = 0, \quad C = \frac{f_0}{\omega_0^2 - \Omega^2}$$

General solution of (*) for $\Omega \neq \omega_0$:

$$q(t) = A \sin(\omega_0 t + \delta) + \frac{f_0 \cos \Omega t}{\omega_0^2 - \Omega^2}$$

A, δ depend on the initial conditions.

Ω -term is in phase with driving force if $\Omega < \omega_0$. If $\Omega > \omega_0$, $q(t)$ oscillates out of phase (phase factor π) with driving force.

$\Omega = \omega_0$:

$$q(t) = A \sin(\omega_0 t + \delta) + \frac{f_0 t \sin \omega_0 t}{2 \omega_0}$$

Forced Damped Oscillator

$$\ddot{q} + 2\beta \dot{q} + \omega_0^2 q = f(t)$$

$\beta = \frac{b}{m}$ is the damping factor

$$(F = \frac{1}{2} b \dot{q}^2, \vec{F}_D = -b \dot{q})$$

$$f(t) = f_0 \cos \Omega t$$

$$q_h(t) = \alpha e^{(-\beta + i\omega)t} \quad \alpha \in \mathbb{C}$$

$\omega = \sqrt{\omega_0^2 - \beta^2}$ is the so-called **natural frequency**

Real solution:

$$e^{-\beta t} [\operatorname{Re} \alpha \cos \omega t - \operatorname{Im} \alpha \sin \omega t]$$

$$\alpha = a e^{i\delta} \text{ where } \alpha, \delta \in \mathbb{R}$$

$$\Rightarrow \operatorname{Re} q_n(t) = a e^{-\beta t} \cos(\omega t + \delta)$$

\Rightarrow Complex phase δ of α is the **physical phase** of the oscillation.

The complex solution:

$$f = f_0 e^{i\Omega t}$$

$$q(t) = \alpha e^{-(\beta + i\omega)t} + \Gamma e^{i\Omega t}$$

(first term: **transient response** ;
second term: **steady state response** ;)

$$\Gamma = \frac{f_0}{\omega_0^2 - \Omega^2 + 2i\beta\Omega}$$

Phase difference γ between the driving force $e^{i\Omega t}$ and Γ is

$$\gamma = \arctan \frac{\operatorname{Im} \left(\frac{f_0}{\Gamma} \right)}{\operatorname{Re} \left(\frac{f_0}{\Gamma} \right)}$$

$$\frac{f_0}{\Gamma} = \omega_0^2 - \Omega^2 + 2i\beta\Omega \Rightarrow \tan \gamma = \frac{2\beta\Omega}{\omega_0^2 - \Omega^2}$$

Steady state amplitude:

$$|\Gamma| = \frac{|f_0|}{\sqrt{(\omega_0^2 - \Omega^2)^2 + 4\beta^2\Omega^2}}$$

$|\Gamma|$ has maximum when

$$\Omega = \sqrt{\omega_0^2 - 2\beta^2}$$

maximum value is

$$\frac{|f_0|}{2\beta}$$

6.RigidBodies

6.1Introduction

6.1.1RigidityandKinematics

Definition: A **rigid body** is an extended collection of point particles so that the distance between any two of them remains constant.

The configuration of the body:

- by position of an arbitrary point (3 coordinate)
- by its orientation relative to the axes of an inertial system (3 angles)

$$\Rightarrow \dim \mathbb{Q} = 6$$

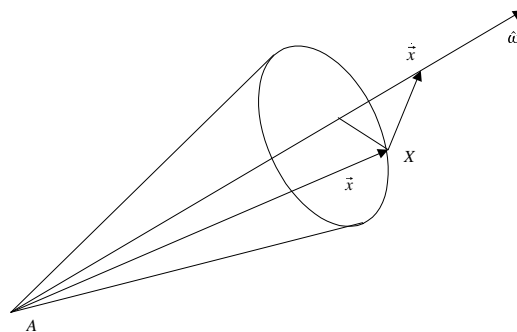
Common: fixed point = pivot

If sum of the external forces vanishes \Rightarrow center of mass does not accelerate, may serve as pivot even if body has no fixed point

Henceforth: assume that there is an **inertial point** A in the body

Describe motion of a rigid body in the inertial frame. Rigidity implies:

- (1) that there is an instantaneous axis of rotation $\hat{\omega}$, i.e. a line in the body that passes through the origin A and is instantaneously at rest.
- (2) all points in the body move at right angles to $\hat{\omega}$ at speeds proportional to their distance from this instantaneous axis



Inertial point $A = \begin{cases} \text{center of mass} \\ \text{pivot} \end{cases}$

$$X \neq A, \vec{x} \cdot |\dot{\vec{x}}| = \text{const}$$

$$\frac{d}{dt} (x^2) = 2 \vec{x} \cdot \dot{\vec{x}} = 0$$

\Rightarrow There must be a line $\hat{\omega}$ in the body that is instantaneously stationary.

$\hat{\omega}$ is instantaneous axis of rotation, speed of X is $\dot{x} = \omega r_x$.

ω : **instantaneous angular speed** or **rate of rotation**

Definition: Instantaneous angular velocity vector :

$$\vec{\omega} : \frac{\vec{\omega}}{|\vec{\omega}|} = \hat{\omega} ; |\vec{\omega}| = \omega ;$$

$$\Rightarrow \dot{\vec{x}} = \vec{\omega} \times \vec{x}$$

6.12 Kinetic Energy and Angular Momentum

In inertial system, origin A . Mass density $\mu(\vec{x})$.

$$T = \frac{1}{2} \int \dot{x}^2(\vec{x}) \mu(\vec{x}) d^3x = \frac{1}{2} \int \dot{x}^2 dm ;$$

$$\dot{x}_k = \varepsilon_{klm} \omega_l x_m ; \quad (\text{implied summation})$$

$$\dot{x}^2 = \dot{x}_k \dot{x}_k = \varepsilon_{klm} \omega_l x_m \varepsilon_{kij} \omega_i x_j = (\delta_{li} \delta_{mj} - \delta_{lj} \delta_{mi}) \omega_l \omega_i x_m x_j = \omega_l (\delta_{li} x^2 - x_l x_i) \omega_i$$

$$T = \frac{1}{2} \omega_l \left[\int (\delta_{li} x^2 - x_l x_i) dm \right] \omega_i = \frac{1}{2} \omega_l I_{li} \omega_i = \frac{1}{2} \vec{\omega} \cdot \overset{\leftrightarrow}{I} \vec{\omega} ;$$

$$I_{li} \equiv \int (\delta_{li} x^2 - x_l x_i) dm$$

are the elements of the **inertia tensor** or **inertia matrix** (G: Trägheitstensor)

$$T = \frac{1}{2} \vec{v} \cdot m \vec{v}$$

$$I > 0 \Rightarrow \exists I^{-1} ; \overset{\leftrightarrow}{I} \text{ is symmetric}$$

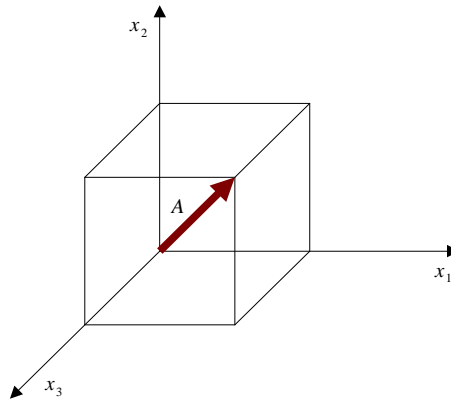
\Rightarrow diagonalize by orthogonal transformation \Rightarrow there is an orthogonal coordinate system whose basis vectors are eigenvectors of $\overset{\leftrightarrow}{I}$. In this coordinate system $\overset{\leftrightarrow}{I}$ is diagonal: **principal axis system** (G: Hauptachsensystem), the eigenvalues of $\overset{\leftrightarrow}{I}$ are called **principal moments** or **moments of inertia** (G: Hauptträgheitsmomente).

$$\overset{\leftrightarrow}{I} = \begin{pmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{pmatrix}$$

$$T = \frac{1}{2} (I_1 \omega_1^2 + I_2 \omega_2^2 + I_3 \omega_3^2)$$

ω_k are the components of $\vec{\omega}$ in the principal axis system.

Example: Uniform cube of side s ; pivot A is a corner.



$$I_{11} = I_{22} = I_{33} = \mu \int_0^s dx_1 \int_0^s dx_2 \int_0^s dx_3 (x_2^2 + x_3^2) = \frac{2}{3} \mu s^5$$

$$I_{12} = I_{23} = I_{31} = -\mu \int_0^s dx_1 \int_0^s dx_2 \int_0^s dx_3 x_1 x_2 = -\frac{1}{4} \mu s^5$$

$$I = \frac{2}{3} M s^2 \begin{pmatrix} 1 & -\frac{3}{8} & -\frac{3}{8} \\ -\frac{3}{8} & 1 & -\frac{3}{8} \\ -\frac{3}{8} & -\frac{3}{8} & 1 \end{pmatrix};$$

$M \equiv \mu s^3 = \text{mass of the cube}$

Eigenvalues and eigenvectors of the matrix

$$A = \begin{pmatrix} 1 & \alpha & \alpha \\ \alpha & 1 & \alpha \\ \alpha & \alpha & 1 \end{pmatrix}, \quad \alpha = -\frac{3}{8}$$

$$\det(A - \lambda E) = 0 = \det \begin{pmatrix} 1 - \lambda & \alpha & \alpha \\ \alpha & 1 - \lambda & \alpha \\ \alpha & \alpha & 1 - \lambda \end{pmatrix}$$

$$= (1 - \lambda)^3 - 3 \alpha^2 (1 - \lambda) + 2 \alpha^3 = (1 - \lambda - \alpha)^2 (1 - \lambda + 2 \alpha)$$

$$\lambda_1 = 2 \alpha + 1 = \frac{1}{4} \Rightarrow \vec{q}_1 = \frac{1}{\sqrt{3}} \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$$

$$\lambda_2 = \lambda_3 = 1 - \alpha = \frac{11}{8} \Rightarrow \vec{q}_2 \perp \vec{q}_3 \perp \vec{q}_1$$

$$\Rightarrow I_1 = \frac{1}{6} M s^2, \quad I_2 = I_3 = \frac{11}{12} M s^2;$$

Angular Momentum

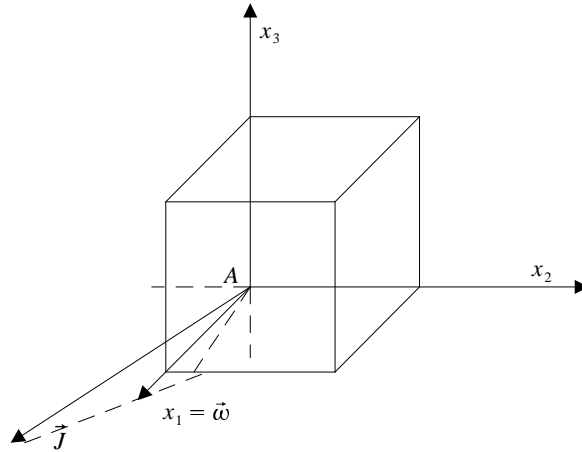
The angular momentum of the rigid body is

$$\vec{J} = \int \mu(\vec{x}) \vec{x} \times \dot{\vec{x}} d^3 x = \int \vec{x} \times \dot{\vec{x}} d m$$

$$[\vec{x} \times (\vec{\omega} \times \vec{x})]_i = \varepsilon_{ijk} x_j \varepsilon_{klm} \omega_l x_m = (\delta_{il} \delta_{jm} - \delta_{im} \delta_{jl}) x_j \omega_l x_m = (\delta_{il} x^2 - x_i x_l) \omega_l$$

$$J_i = I_{il} \omega_l \text{ or } \vec{J} = I \vec{\omega}$$

Example:



$$\vec{\omega} = \begin{pmatrix} \Omega \\ 0 \\ 0 \end{pmatrix}$$

$$\vec{J} = \frac{2}{3} M \varepsilon^2 \begin{bmatrix} 1 & \alpha & \alpha \\ \alpha & 1 & \alpha \\ \alpha & \alpha & 1 \end{bmatrix} \begin{bmatrix} \Omega \\ 0 \\ 0 \end{bmatrix} = M \varepsilon^2 \Omega \begin{pmatrix} \frac{2}{3} \\ -\frac{1}{4} \\ -\frac{1}{4} \end{pmatrix}$$

6.1.3 Dynamics

The equation for rigid body motion was (2.4.5):

$$N_Z = \vec{J}_Z$$

Z : both vectors must be calculated about the center of mass or about a pivot

Space and Body System

1) A non-inertial system, called the **body system** B , is fixed in the body and moves with it.

Note: We shall denote column vectors that contain the components of a vector in a given coordinate system without an arrow. Since the components x_B of the position vector \vec{x} of any point in the body are fixed, $\dot{x}_B = 0$.

2) An inertial system, called the **space system** S . We write x_S for the representation of \vec{x} in S and $\dot{x}_S \neq 0$.

Both origins are at A (inertial point). For some time both coordinates coincide.

Suppose some such coordinate system is specified. Then \vec{x} is fixed in the body, $\dot{\vec{x}}$ is the rate of

change viewed from the specified system and $\vec{\omega}$ is the angular velocity of the body with respect to the specified system.

In particular, if the system S that coincides instantaneously with B , $\dot{\vec{x}} = \vec{\omega} \times \vec{x}$ reads
 $\dot{x}_S = \omega_B \times x_B$ (*)

We can extend (*) to an arbitrary vector \vec{s} in the body, one that may be moving in the body system B . Its velocity \dot{s}_S relative to the inertial system S is the velocity $\omega \times s_B$ it would have if it were fixed in B and velocity \dot{s}_B relative to B :

$$\dot{s}_S = \omega_B \times s_B + \dot{s}_B (**)$$

Tells us how to transform velocity vectors between B and S .

If \dot{s} in this equation is angular velocity,

$$\omega_S = \underbrace{\omega_B \times \omega_B}_{=0} + \omega_B = \omega_B$$

\Rightarrow The body and space representations of $\vec{\omega}$ and $\dot{\vec{\omega}}$ are identical.

Dynamical Equations

If (**) is applied to $\dot{s} \rightarrow \dot{J}$

$$\dot{J}_S = \omega \times J_B + \dot{J}_B = \omega \times (I_B \omega) + I_B \dot{\omega}$$

\Rightarrow Equations of motion reads $N_S = \omega \times (I_\omega) + I \dot{\omega}$.

In the principal axis system, this reads

$$N_1 = (I_3 - I_2) \omega_3 \omega_2 + I_1 \dot{\omega}_1$$

$$N_2 = (I_1 - I_3) \omega_1 \omega_3 + I_2 \dot{\omega}_2$$

$$N_3 = (I_2 - I_1) \omega_2 \omega_1 + I_3 \dot{\omega}_3$$

Euler Equations

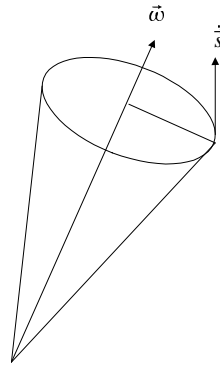
Rigid bodies: 6 degrees of freedom

Inertial point, pivot:

- remains fixed
- center of mass

$$\left(\frac{d \vec{s}}{d t} \right)_S = \left(\frac{d \vec{s}}{d t} \right)_B + \vec{\omega} \times \vec{s}$$

$\vec{\omega}$ instantaneous angular velocity



$$\vec{N}_Z = \frac{d}{d t_S} (\vec{J}_Z) = \frac{d}{d t_S} (\overset{\leftrightarrow}{I} \vec{\omega})$$

\vec{J}_Z = angular momentum

$\overset{\leftrightarrow}{I}$ = inertial tensor

Written in body system: $\overset{\leftrightarrow}{I} = \text{cent}$

$$\vec{N}_B = \frac{d}{d t_B} \vec{J}_B + \vec{\omega}_B \times \vec{J}_B = \overset{\leftrightarrow}{I} \cdot \dot{\vec{\omega}} + \vec{\omega} \times (\overset{\leftrightarrow}{I} \vec{\omega})$$

Principal axis system:

$$\overset{\leftrightarrow}{I} = \begin{pmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{pmatrix}$$

$$N_1 = (I_3 - I_2) \omega_3 \omega_2 + I_1 \dot{\omega}_1$$

$$N_2 = (I_1 - I_3) \omega_1 \omega_3 + I_1 \dot{\omega}_2$$

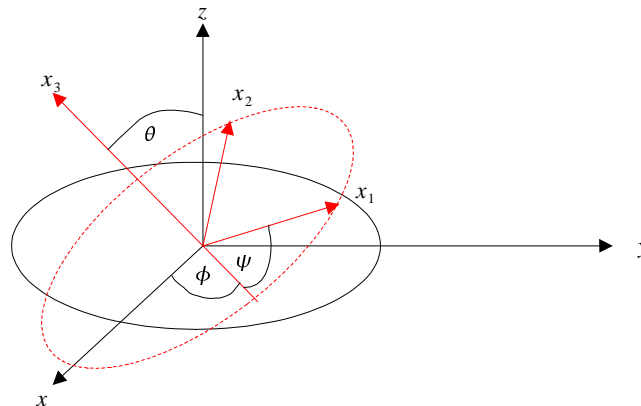
$$N_3 = (I_2 - I_1) \omega_2 \omega_1 + I_1 \dot{\omega}_3$$

Euler Angles

let x, y, z denote axes of *spacesystem*

$x_1, x_2, x_3 \sim \text{bodysystem}$

ϕ, ψ, θ



$$(x, y, z) \leftrightarrow (x_1, x_2, x_3)$$

Rotation through finite angles: not commutative!

Angular velocity vectors are commutative.

Therefore, $\vec{\omega} = \vec{\Theta} + \vec{\Phi} + \vec{\Psi}$

Euler angular velocity vectors are directed along their instantaneous axes of rotation:

$\vec{\Psi} \parallel x_3$, $\vec{\Phi} \parallel z$, $\vec{\Theta} \parallel$ modalline of 2 planes

$\vec{\omega} = (\omega_x, \omega_y, \omega_z)$ in space system

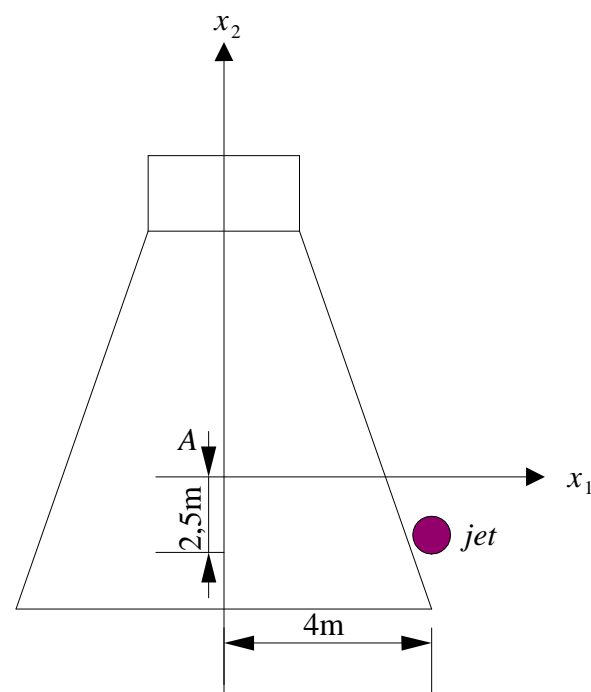
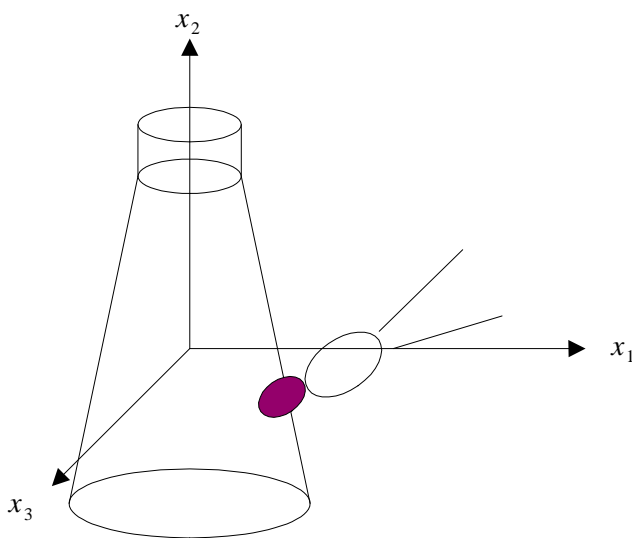
$\vec{\omega} = (\omega_1, \omega_2, \omega_3)$ in body system

$\omega_1 = \dot{\phi} \sin \theta \sin \psi + \dot{\theta} \cos \psi$

$\omega_2 = \dot{\phi} \sin \theta \cos \psi - \dot{\theta} \sin \psi$

$\omega_3 = \dot{\phi} \cos \theta + \dot{\psi}$

6.1.4 Example: Jet-Driven Spacecraft



$m = 2000 \text{ kg}$

radii of gyration $\varrho_{x_1} = \varrho_{x_3} = 1,5 \text{ m}$; $\varrho_{x_2} = 1,75 \text{ m}$

\Leftrightarrow the principal moment of inertia in x -direction is $I_1 = m \varrho_{x_1}^2, I_2 = m \varrho_{x_2}^2, I_3 = m \varrho_{x_3}^2$

Initially, the spacecraft is at rest. Then, the jet fires for 1 s. It has a thrust of 25 N that acts parallel to the x_3 -axis.

– Axis of precession?

– Angular velocity and the rates of precession after the jet has stopped?

1st part: let $t = 0$ be the time when the rocket is turned on. We use the *body system*.

$$\vec{M} = I \vec{\dot{\omega}} + \vec{\omega} \times (I \vec{\omega}) = I_1 \omega_1 \vec{e}_1 + I_2 \omega_2 \vec{e}_2 + I_3 \omega_3 \vec{e}_3 + O(\omega^2)$$

$\omega^2 \ll \dot{\omega}$ during that 1 s.

$$\vec{M} = \vec{r} \times \vec{F} = (s_1 \vec{e}_1 - s_2 \vec{e}_2) \times F \vec{e}_3; (s_1, s_2) = (4 \text{ m}, 2.5 \text{ m});$$

$$\vec{M} = -s_2 F \vec{e}_1 - s_1 F \vec{e}_2$$

$$\Rightarrow \dot{\omega}_1 = -s_2 \frac{F}{I_1} = -C_1$$

$$\Rightarrow \dot{\omega}_2 = -s_1 \frac{F}{I_2} = -C_2$$

$$\Rightarrow \dot{\omega}_3 = 0$$

$$t = 0 : \omega_i(0) = 0$$

$$\omega_1(t) = -C_1 t$$

$$\omega_2(t) = -C_2 t$$

$$\omega_3(t) = 0$$

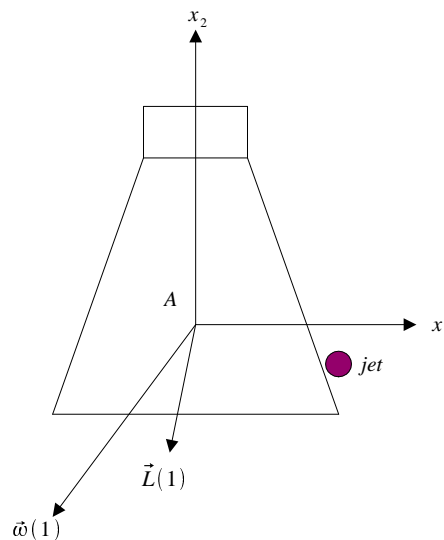
After 1 s:

$$\omega_1(1) = \frac{-2.5 \text{ m} \cdot 25 \text{ N}}{2000 \text{ kg} (1.5 \text{ m})^2} \cdot 1 \text{ s} = -0.0139 \text{ rad/s}$$

$$\omega_2(1) = -0.0163 \text{ rad/s}$$

$$\omega^2 = \omega_1^2 + \omega_2^2 \Rightarrow |\vec{\omega}(1)| = 0.02 \text{ rad/s}$$

$$\tan \varphi = \frac{\omega_1}{\omega_2} = 0.85 \Rightarrow \varphi(1) = 44,5^\circ$$



The capsule is rotating around a momentary axis that points along the negative 1- and 2-direction.

$$\vec{L} = I_1 \omega_1 \vec{e}_1 + I_2 \omega_2 \vec{e}_2 + I_3 \omega_3 \vec{e}_3$$

$$\vec{L}(1) = -2000 (1.5)^2 (0.0139) \vec{e}_1 - 2000 (1.75)^2 (0.0163) \vec{e}_2$$

$$\tan \Theta = \frac{L_1}{L_2} = 0.63 \Rightarrow \Theta(1) = 32^\circ$$

2. part

Motion after rocket has stopped. $t = 0$

$\vec{\omega}(1), \vec{L}(1)$ became initial values for the subsequent motion.

Remain in body system: $\vec{M} = 0$

i.e. $\left(\frac{d\vec{L}}{dt}\right)_{\text{Space system}} = 0 \Rightarrow \vec{L}$ does not change in the *space system*.

$$I_1 \dot{\omega}_1 + (I_3 - I_2) \omega_2 \omega_3 = 0$$

$$I_2 \dot{\omega}_2 + (I_1 - I_3) \omega_1 \omega_3 = 0$$

$$I_3 \dot{\omega}_3 + (I_2 - I_1) \omega_1 \omega_2 = 0$$

$$I_1 = I_3 \Rightarrow \dot{\omega}_2 = 0 \Rightarrow \omega_2(t) = \omega_2(0) = -0.0163 \text{ rad/s}$$

$$A = \frac{I_2 - I_1}{I_1}; B = \omega_2(0); \Rightarrow$$

$$\dot{\omega}_1 - A B \omega_3 = 0$$

$$\dot{\omega}_3 + A B \omega_1 = 0$$

$$\omega_1 = \alpha e^{k t}, \omega_3 = \beta e^{k t}$$

\Rightarrow

$$\omega_1(t) = C \cos(\gamma t + \theta)$$

$$\omega_3(t) = -C \sin(\gamma t + \theta), \gamma = A B$$

$$t = 0: \omega_1(0) = -0.0139 \text{ rad/s}, \omega_3(0) = 0$$

$$\Rightarrow \theta = 0$$

$$\omega_1(t) = \omega_1(0) \cos \gamma t$$

$$\omega_3(t) = \omega_1(0) \sin \gamma t$$

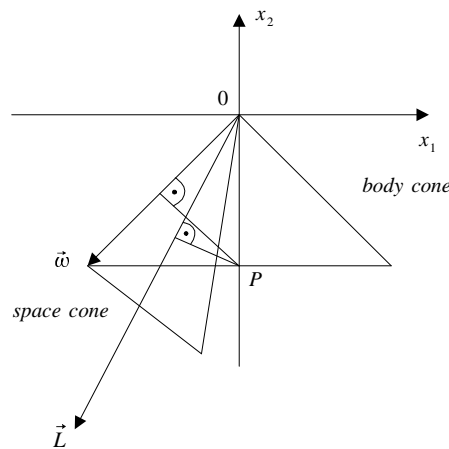
$$\gamma = A B$$

$$\omega_1^2(t) + \omega_3^2(t) = \omega_1^2(0)$$

Rotation about x_2 -axis in the (x_1, x_2) -plane, $\vec{\omega}$ also maintains its initial angular displacement φ with respect to the x_2 -axis. The cone that traces out is called the **body cone** („Polkegel“): motion is with respect to (x_1, x_2, x_3) fixed in the body.

Frequency of rotation around the x_2 -axis: $P = A B = -0.0059 \text{ rad/s}$; \vec{L} stays fixed.

Inertial system: $\vec{\omega}$ rotates around \vec{L} with a frequency of rotation Ω . This motion also generates a cone called the **space cone** („Spurkegel“).



These cones have always a common line of contact. Thus, $\vec{\omega}$ acts as an instantaneous axis and the general motion can be characterized by noting that the body cone rolls on the fixed space cone.

Calculate rotation frequency Ω :

P will turn through a distance $ds = a \omega dt$ about $\vec{\omega}$. It will also turn through a distance $ds = b \Omega dt$ with respect to L . \Rightarrow

$$a \omega = b \Omega \Rightarrow \Omega = \omega \frac{\sin \varphi}{\sin \theta} = 0.2616 \frac{\text{rad}}{\text{s}}.$$

6.2 Lagrange Equations for Rigid Bodies

$$\frac{d}{dt} (\overset{\leftrightarrow}{I} \vec{\omega}) = \vec{M}$$

efficient only if $\vec{M} = 0$ or fixed in body.

We consider pivoted bodies and take the origin of the body system in that pivot.

Pivot = X (center of mass) \Rightarrow rotational and translational motion are decoupled

Pivot = fixed \Rightarrow only rotation

We choose 3 Euler angles ϕ, ψ, θ as generalized coordinates. We assume that the potential energy depends only on those coordinates and on time. Then

$$L(\phi, \psi, \theta, \dot{\phi}, \dot{\psi}, \dot{\theta}) = T_{rot} - U = \frac{\vec{\omega} \cdot (\overset{\leftrightarrow}{I} \vec{\omega})}{2} - U(\phi, \psi, \theta, t)$$

In principal axes, we have, in terms of the body-system components I_i and ω_i

$$T_{rot} = \frac{I_1 \omega_1^2 + I_2 \omega_2^2 + I_3 \omega_3^2}{2}$$

$$L(\phi, \psi, \theta, \dot{\phi}, \dot{\psi}, \dot{\theta}) = \frac{I_1}{2} (\dot{\phi} \sin \theta \sin \psi + \dot{\theta} \cos \psi)^2 + \frac{I_2}{2} (\dot{\phi} \sin \theta \cos \psi - \dot{\theta} \sin \psi)^2 + \frac{I_3}{2} (\dot{\phi} \cos \theta + \dot{\psi})^2 - U(\phi, \psi, \theta, t)$$

7. Hamiltonian Formulation of Mechanics

In some cases, a system becomes easier to understand and to discuss by choosing the generalized coordinates q^α and the generalized momenta p^α rather than q^α and \dot{q}^α as independent variables. Such a change in variables produces pairs of first-order rather than second-order ODEs.

$$p_\alpha = \frac{\partial L}{\partial \dot{q}^\alpha} \quad (*)$$

$$\frac{d}{dt} p_\alpha = \frac{\partial L}{\partial q^\alpha} \quad (**)$$

$$\frac{d q^\alpha}{dt} = \dot{q}^\alpha$$

L, \dot{q} are all functions of (q, \dot{q}, t) rather than of (q, p, t) . Assume we can invert (*) to get \dot{q} in terms of (q, p, t) . The right hand side of (**) can be transformed: Replace \dot{q} in $\partial L / \partial q$ by $\dot{q}^\alpha(q, p, t)$. The partial derivative of $L(q, \dot{q}, t)$ with respect to q^α is not the same as that of $\hat{L}(q, p, t) = L(q, \dot{q}(q, p, t), t)$.

$$\frac{\partial \hat{L}}{\partial q^\alpha} = \frac{\partial L}{\partial q^\alpha} + \frac{\partial L}{\partial \dot{q}^\beta} \frac{\partial \dot{q}^\beta}{\partial q^\alpha} = \frac{\partial L}{\partial q^\alpha} + p_\beta \frac{\partial \dot{q}^\beta(q, p, t)}{\partial q^\alpha}$$

$$\frac{\partial L}{\partial q^\alpha} = \frac{\partial}{\partial q^\alpha} \left[\hat{L}(q, p, t) - p_\beta \dot{q}^\beta(q, p, t) \right]$$

The derivative of \hat{L} with respect to p_α :

$$\frac{\partial \hat{L}}{\partial p_\alpha} = \frac{\partial L}{\partial \dot{q}^\beta} \frac{\partial \dot{q}^\beta}{\partial p_\alpha} = p_\beta \frac{\partial \dot{q}^\beta}{\partial p_\alpha}$$

$$\frac{\partial}{\partial p_\alpha} \left[\hat{L}(q, p, t) - p_\beta \dot{q}^\beta(q, p, t) \right] = -\dot{q}^\alpha$$

Definition: $H(q, p, t) \equiv p_\beta \dot{q}^\beta(q, p, t) - \hat{L}(q, p, t)$ is called the **Hamiltonian function** or the **Hamiltonian**.

For many dynamical systems: $E = H = T + V$ where $L = T - V$.

$$\dot{q}^\beta = \frac{\partial H(q, p, t)}{\partial p_\beta}, \quad \dot{p}_\beta = -\frac{\partial H}{\partial q^\beta}$$

Hamilton's canonical equations: A set of equations of motion in the Hamiltonian formalism.

$(q(t), p(t))$ -manifold.

The term „canonical“ means *standard* or *conventional*.

Examples:

1) The Lagrangian of a particle in a potential

$$L = \frac{m}{2} (\dot{x}_1^2 + \dot{x}_2^2 + \dot{x}_3^2) - V(x_1, x_2, x_3, t)$$

$$p_i = \frac{\partial L}{\partial \dot{x}_i} = m \dot{x}_i$$

$$H(x, p, t) = \sum_i p_i \frac{p_i}{m} - \frac{m}{2} \sum_i \frac{p_i^2}{m^2} + V(x, t) = \frac{1}{2m} (p_1^2 + p_2^2 + p_3^2) + V(x, t) = T + V$$

$$\dot{p}_i = -\frac{\partial H}{\partial x_i} = -\frac{\partial V}{\partial x_i} = F_i$$

$$\dot{x}_i = \frac{\partial H}{\partial p_i} = \frac{p_i}{m}$$

$$\Leftrightarrow m \ddot{\vec{x}} = -\text{grad } V$$

2) The Lagrangian in an electromagnetic field was

$$L(q, \dot{q}, t) = \frac{1}{2} m \dot{q}^\beta \dot{q}^\beta - e \varphi(q, t) + e \dot{q}^\beta A_\beta(q, t)$$

($\beta = 1, 2, 3$ implied summations)

The generalized momentum p_y that is **canonically conjugate** to q^y .

$$p_y = m \dot{q}^y + e A_y$$

This canonically conjugate momentum is not equal to the dynamical momentum $m \dot{q}^y$ but has an additional contribution from A .

$$\Rightarrow H(q, p, t) = \frac{1}{2m} \delta^{\alpha\gamma} \{p_\alpha - e A_\alpha(q, t)\} \{p_\gamma - e A_\gamma(q, t)\} + e \varphi(q, t);$$

$$H = \frac{1}{2m} (\vec{p} - e \vec{A})^2 + e \varphi(q, t)$$

$$\Rightarrow m \ddot{\vec{q}} = \vec{F} = e (\vec{v} \times \vec{B} + \vec{E}),$$

$$\vec{E} = -\vec{\nabla} \varphi - \frac{\partial \vec{A}}{\partial t},$$

$$\text{curl } \vec{A} = \vec{B}$$

7.1 A Brief Review of Special Relativity

quantum mechanics: $\hbar \rightarrow 0$ \rightarrow classical mechanics

relativity: $c \rightarrow \infty$ \rightarrow classical mechanics

Einstein's special theory of relativity: compares the way a physical system is described by different observers moving at *constant velocity* with respect to each other.

Galilean transformation ($V \ll c$): One observer sees a certain event \vec{x}, t ; second observer

$$\vec{V} : \vec{x}', t';$$

$$\vec{x}' = \vec{x} - \vec{V} t, t' = t$$

Lorentz transformation ($\vec{V} \parallel x_1$ -axis):

$$x'^1 = \gamma \left[x^1 - \frac{V x^0}{c} \right], x'^0 = \gamma \left[x^0 - \frac{V x^1}{c} \right], x'^2 = x^2, x'^3 = x^3, x^0 \equiv c t, \gamma = \frac{1}{\sqrt{1 - V^2/c^2}}$$

Introduce 4-vectors $x = (x^0, x^1, x^2, x^3)$ ($c = 1$, light years for distance)

The geometry of the 4D-space-time-manifold is called **Minkowskian**.

In **Euclidean** geometry

$$\Delta s^2 = (\Delta x^1)^2 + (\Delta x^2)^2 + (\Delta x^3)^2$$

is invariant, where $\Delta \vec{x}$ is the separation between two points.

In Minkowski geometry:

$$\Delta \sigma^2 \equiv g_{\mu\nu} \Delta x^\mu \Delta x^\nu = -(\Delta x^0)^2 + (\Delta x^1)^2 + (\Delta x^2)^2 + (\Delta x^3)^2$$

where $\Delta x \equiv (\Delta x^0, \Delta x^1, \Delta x^2, \Delta x^3)$ is the space-time separation between two **events**.

$$\mu = 0, 1, 2, 3.$$

Minkowskian metric $g_{\mu\nu} = 0$ if $\mu \neq \nu$; $g_{11} = g_{22} = g_{33} = -g_{00} = 1$

Special relativistic generalization of Newton's equations is

$$m \frac{d^2 x^\mu}{d\tau^2} \equiv m a^\mu = F^\mu \left(x, \frac{dx}{d\tau}, \tau \right)$$

x, a, F are four-vectors. The mass (called the **rest mass**) is a scalar. The scalar τ is called the **proper time** („Eigenzeit“): it is measured along the motion and is defined by

$$(d\tau)^2 = -g_{\mu\nu} dx^\mu dx^\nu$$

$$-(d\tau)^2 = (dx^1)^2 + (dx^2)^2 + (dx^3)^2 - dt^2 = \vec{v}^2 dt^2 - dt^2 = -(1 - \vec{v}^2) dt^2$$

$$d\tau = \frac{dt}{\gamma}, \quad \gamma = \frac{1}{\sqrt{1 - \vec{v}^2/c^2}}$$

4-vector generalization of the 3-vector velocity has components

$$u^\mu = \frac{dx^\mu}{d\tau}, \quad g_{\mu\nu} u^\mu u^\nu = -1$$

\Rightarrow velocities are limited in magnitude

$$u^0 = \gamma$$

$$u^k = \gamma v^k \equiv \gamma \frac{dx^k}{dt} \quad k = 1, 2, 3$$

v^k is the nonrelativistic velocity

Want to find Hamiltonian of this relativistic dynamics:

$$L_R = T(\vec{v}) - U(\vec{x})$$

T, U are relativistic generalizations of the kinetic and potential energies, \vec{v} and \vec{x} are the 3-vectors.

The 3-velocity should satisfy the equation

$$\frac{\partial L_R}{\partial v^k} = p^k$$

(Latin indices go from 1 to 3, Greek indices from 0 to 3)

$$p^k = m u^k = m \gamma v^k = \frac{m v^k}{\sqrt{1 - \vec{v}^2}}, \quad p^0 = m \gamma$$

where $\vec{v}^2 = (v^1)^2 + (v^2)^2 + (v^3)^2$. \vec{v} is the 3-velocity of the particle.

$$\frac{\partial T}{\partial v^k} = \frac{m v^k}{\sqrt{1 - \vec{v}^2}}$$

$$\Rightarrow T = -m \sqrt{1 - \vec{v}^2} + C = \frac{-m}{\gamma} + C;$$

$$v \ll c \Rightarrow T \approx \frac{1}{2} m \vec{v}^2 + u$$

Relativistic Lagrangian of a conservative one-particle system is

$$L_R = -\frac{m}{\gamma} - U(\vec{x})$$

Relativistic expression for energy

$$E_R = \frac{\partial L_R}{\partial v^k} v^k - L_R = p^k v^k - L_R = p^k v^k - L_R = m \gamma \vec{v}^2 + \frac{m}{\gamma} + U(\vec{x})$$

$$= m \gamma \left(1 - \frac{1}{\gamma^2}\right) + \frac{m}{\gamma} + U(\vec{x}) = m \gamma + U(\vec{x})$$

$$\Rightarrow H_R = \frac{\partial L_R}{\partial v^k} v^k - L_R = \frac{p^k p^k}{m \gamma} + \frac{m}{\gamma} + U(\vec{x}),$$

$$\gamma = \frac{1}{\sqrt{1 - \vec{v}^2}} = \sqrt{1 + \frac{\vec{v}^2}{1 - \vec{v}^2}} = \sqrt{1 + \gamma^2 \vec{v}^2}$$

$$m \gamma = \sqrt{\vec{p}^2 + m^2} \quad \vec{p}^2 \equiv p^k p^k$$

\Rightarrow

$$H_R = \sqrt{\vec{p}^2 + m^2} + U(\vec{x})$$

6.1.1 The Relativistic Kepler Problem

We take

$$U = -\frac{e^2}{r}.$$

1916 Sommerfeld obtains correct first-order expressions for the fine structure of the hydrogen spectrum.

$$H = \sqrt{\vec{y}^2 + m^2} - \frac{e^2}{r}, \quad r^2 = \vec{x} \cdot \vec{x}$$

Motion is constrained to a plane \Rightarrow number of freedoms is 2: r, φ

$$H = \sqrt{p_r^2 + \frac{p_\varphi^2}{r^2} + m^2} - \frac{e^2}{r}, \quad p_\varphi = \frac{\partial L}{\partial \dot{\varphi}}, \quad p_r = \frac{\partial L}{\partial \dot{r}}$$

φ is again cyclic $\Rightarrow p_\varphi = \text{conserved}$

$r = r(\varphi)$ instead of $r = r(t), \varphi = \varphi(t)$

Hamiltonian equations of motion \Rightarrow

$$r = \frac{q}{1 + \varepsilon \cos[\Gamma(\varphi - \varphi_0)]}$$

where ε, Γ, q depend on e, c, p_φ and the total energy E .

$$\Gamma = \sqrt{1 - \frac{e^2}{c^2 p_\varphi^2}} \neq 1$$

$r = r(\varphi)$ is *not* a conic section, i.e. the orbit does not close. Orbit looks like a precessing ellipse.

precessing ellipse .

7.2 Canonical Transformations

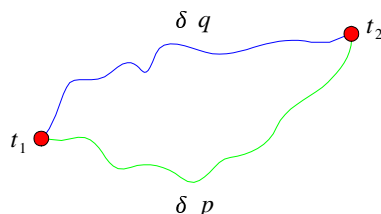
7.2.1 Hamilton's Principle

$$\delta S [q] = \delta \int_{t_1}^{t_2} dt L = \delta \int_{t_1}^{t_2} dt (p_\alpha \dot{q}_\alpha - H(q, p, t)) = 0$$

$$\alpha = 1, \dots, n \quad S = S[q], q(t_1), q(t_2)$$

$S[q, p]$ For given boundary values

$$\delta q(t_1) = \delta q(t_2) = 0, \delta p(t_1) = \delta p(t_2) = 0$$



$$\delta S [q, p] = \int_{t_1}^{t_2} dt \left[\left(\dot{q}_\alpha - \frac{\partial H}{\partial p_\alpha} \right) \delta p^\alpha - \left(\dot{p}_\alpha + \frac{\partial H}{\partial q_\alpha} \right) \delta q^\alpha \right]$$

used:

$$\int p_\alpha \delta \dot{q}_\alpha dt = - \int \dot{p}_\alpha \delta q_\alpha dt$$

Hamiltonian equations of motion $\Leftrightarrow \delta S = 0$

$$\delta S [q, p] = 0 \quad \text{Hamilton's Principle}$$

Because we have $\delta q = 0$ and $\delta p = 0$ at the boundaries, we can add

$$\frac{d}{dt} F(q, p, t),$$

the transformation

$$p_\alpha \dot{q}_\alpha - H \rightarrow p_\alpha \dot{q}_\alpha - H + \frac{d}{dt} F(q, p, t)$$

leaves the canonical equations of motion invariant.

7.2.2 Choice of Coordinates and Momenta

Can we introduce new coordinates and momenta in such a way that the canonical equations have the same form but are easier to solve? Can we find a function $H'(q, p, t)$ such that

$$Q_\alpha = Q_\alpha(q, p, t), \quad P_\alpha = P_\alpha(q, p, t) \quad (\text{canonical transformation})$$

that do:

$$\dot{q}_\alpha = \frac{\partial H}{\partial p_\alpha}, \quad \dot{p}_\alpha = -\frac{\partial H}{\partial q_\alpha}$$

into:

$$\dot{Q}_\alpha = \frac{\partial H'}{\partial P_\alpha}, \quad \dot{P}_\alpha = -\frac{\partial H'}{\partial Q_\alpha}$$

?

$$\delta \int_{t_1}^{t_2} dt (p_\alpha \dot{q}_\alpha - H(q, p, t)) = \delta \int_{t_1}^{t_2} dt (P_\alpha \dot{Q}_\alpha - H'(Q, P, t)) = 0$$

$$\Rightarrow p_\alpha \dot{q}_\alpha - H = P_\alpha \dot{Q}_\alpha - H' + \frac{d}{dt} F(q, p, Q, P, t)$$

Function F is called **generating function** of the transformation.

F depends only on 3 sets of independent variables such as q, P, t or q, Q, t .

Let us choose $F = F(q, Q, t)$:

$$\frac{d}{dt} F(q, Q, t) = \frac{\partial F}{\partial q_\alpha} \dot{q}_\alpha + \frac{\partial F}{\partial Q_\alpha} \dot{Q}_\alpha + \frac{\partial F}{\partial t} \Rightarrow$$

$$p_\alpha = \frac{\partial F(q, Q, t)}{\partial q_\alpha} = p_\alpha(q, Q, t)$$

$$P_\alpha = -\frac{\partial F(q, Q, t)}{\partial Q_\alpha} = P_\alpha(q, Q, t)$$

$$H'(Q, P, t) = H(q, p, t) + \frac{\partial F(q, Q, t)}{\partial t}$$

Example: The Hamiltonian of a harmonic oscillator is

$$H = \frac{p^2}{2m} + \frac{m\omega^2 q^2}{2} \Leftrightarrow \dot{q} = \frac{p}{m}, \dot{p} = -m\omega^2 q$$

For the generating function

$$F(q, Q) = \frac{m\omega}{2} q^2 \cot Q$$

$$p = \frac{\partial F}{\partial q} = m\omega q \cot Q$$

$$P = -\frac{\partial F}{\partial Q} = \frac{m\omega q^2}{2 \sin^2 Q}$$

Can be inverted to give

$$q = \sqrt{\frac{2P}{m\omega}} \sin Q, \quad p = \sqrt{2m\omega P} \cos Q$$

$$H'(Q, P) = H(q(Q, P), p(Q, P)) = \omega P \cos^2 Q + \omega P \sin^2 Q = \omega P$$

The new variable Q is cyclic. The canonical equations are

$$\dot{P} = -\frac{\partial H'}{\partial Q} = 0, \quad \dot{Q} = \frac{\partial H'}{\partial P} = \omega$$

$$\Rightarrow P = \text{const} = \frac{H'}{\omega} = \frac{E}{\omega}; \quad Q(t) = \omega t + \beta;$$

7.3 Hamilton-Jacobi-Equation

Can we find a canonical transformation $W(q, Q, t)$ such that

$$(*) \quad H'(Q, P, t) = H(q, p, t) + \frac{\partial W}{\partial t} = 0?$$

Condition leads to a PDE for W that is called the **Hamilton-Jacobi equation**. It is ideally suited for studying the relations between mechanics, optics, quantum mechanics. The equation (*) obeys:

$$p_\alpha = \frac{\partial W(q, Q, t)}{\partial q^\alpha} = p_\alpha(q, Q, t)$$

$$P_\alpha = -\frac{\partial W(q, Q, t)}{\partial Q^\alpha} = P_\alpha(q, Q, t)$$

$$H' = 0 \Rightarrow \dot{Q}_\alpha = 0, \dot{P}_\alpha = 0 \Rightarrow Q_\alpha = a_\alpha = \text{const}, P_\alpha = b_\alpha = \text{const}$$

Hamilton-Jacobi equation :

$$H\left(q_\alpha, \frac{\partial W(q, a, t)}{\partial q_1}, \dots, \frac{\partial W(q, a, t)}{\partial q_n}, t\right) + \frac{\partial W(q, a, t)}{\partial t}$$

Assume we have solved this PDE and found

$$W(q_1, q_2, \dots, q_n, a_1, \dots, a_n, t)$$

that depend on n constants of integration a_α . This solution leads to the equation

$$p_\alpha = \frac{\partial W(q, a, t)}{\partial q^\alpha} \xrightarrow{\text{inversion}} q_\alpha = q_\alpha(a, b, t)$$

$$b_\alpha = -\frac{\partial W(q, a, t)}{\partial a^\alpha} \xrightarrow{\text{inversion}} p_\alpha = p_\alpha(a, b, t)$$

If H does not explicitly depend on time,

$$W(q, a, t) = S(q, a) - E t$$

$$H\left(q_\alpha, \frac{\partial S(q, a)}{\partial q^\alpha}\right) = E$$

Example (cone on a tilted plane (homework)) :

$$H = \frac{1}{2m} (p_x^2 + p_z^2) + m g z$$

$$\frac{1}{2m} \left(\frac{\partial S(x, z)}{\partial x}\right)^2 + \frac{1}{2m} \left(\frac{\partial S(x, z)}{\partial z}\right)^2 + m g z = E$$

PDE Ansatz:

$$S(x, z) = S_1(x) + S_2(z)$$

$$\left(\frac{dS_1}{dx}\right)^2 + \left(\frac{dS_2}{dz}\right)^2 + 2m^2 g z = 2mE \text{ or}$$

$$\left(\frac{dS_1}{dx}\right)^2 = f(z) = \text{const} = a_2$$

$$\frac{dS_1}{dx} = \sqrt{a_2}$$

$$\frac{dS_2}{dz} = \sqrt{2mE - a_2 - 2m^2 g z}$$

$$S_1 = \sqrt{a_2} x$$

$$S_2 = -\frac{1}{3m^2 g} (2mE - a_2 - 2m^2 g z)^{\frac{3}{2}}$$

$$S = S(x, z, E, a_2) = \sqrt{a_2} x - \frac{1}{3 m^2 g} (2 m E - a_2 - 2 m^2 g z)^{\frac{3}{2}}$$

$$p_x = \frac{\partial S}{\partial x}, p_z = \frac{\partial S}{\partial z}, b_1 = -\frac{\partial S}{\partial E} + t, b_2 = -\frac{\partial S}{\partial a_2}$$

$$\Rightarrow x(t), z(t), p_x(t), p_z(t)$$

$$-\frac{1}{m g} \sqrt{2 m E - a_2 - 2 m^2 g z} = t - b_1$$

$$\Rightarrow z(t) = -\frac{g}{z} (t - b_1)^2 + \frac{2 m E - a_2}{2 m^2 g} = -\frac{g}{2} t^2 + c_1 t + c_2$$

\Rightarrow parabola

8. Nonlinear Dynamics

8.1 Introduction

Irregular, unpredictable time evolution = „chaos“

Chaotic dynamical systems are deterministic.

For non-chaotic systems: slight change in initial conditions leads to differences in the phase space trajectories that grow *linearly* in time.

For a chaotic system, the error grows *exponentially* in time.

⇒ „Sensitivity to initial conditions.“ (1913 Poincaré)

For chaos, the irregularity is not caused by random forces, but is part of the intrinsic dynamics of the deterministic system.

Necessary conditions for chaotic motion :

(a) the system has at least 3 independent dynamical variables

(b) the equations of motion contain a *nonlinear* term that couples at least 2 of the variables

Example: damped, sinusoidally driven pendulum of mass m (weight W) and length l :

$$m l^2 \frac{d^2 \theta}{dt^2} + \gamma \frac{d\theta}{dt} + W l \sin \theta = A \cos(\omega_D t)$$

In dimensionless form:

$$\frac{d\theta}{dt^2} + \frac{1}{q} \frac{d\theta}{dt} + \sin \theta = g \cos(\omega_D t)$$

q is the damping (or quality) parameter, g is the forcing amplitude, ω_D is the drive frequency.

Rewrite:

$$\frac{d\omega}{dt} = -\frac{1}{q} \omega - \sin \theta + g \cos \phi$$

$$\frac{d\phi}{dt} = \omega_D$$

$$\frac{d\theta}{dt} = \omega$$

ϕ is the phase of the drive term. 3 variables (ω, θ, ϕ).

8.2 Tools for Chaotic Systems

8.2.1 Phase Space

Phase space: diagram (\vec{x}, \vec{v}) or (\vec{x}, \vec{p})

Undamped pendulum in small amplitude approximation: $\sin \theta \approx \theta$

$$\frac{d^2 \theta}{dt^2} + \theta = 0; \quad \omega \equiv \frac{d\theta}{dt} \Rightarrow$$

$$\frac{d\omega}{dt} = -\theta, \quad \frac{d\theta}{dt} = \omega \Rightarrow \theta = a \cos t, \quad \omega = a \sin t.$$

In a *deterministic* system, trajectories have the following properties:

(a) Orbits do not cross each other.

(b) Conservative deterministic systems *preserve areas* in phase space, i.e. all points in a given area of phase space move in such a way that these points occupy the same area at all times.

The property of volume/area preservation leads to a classification of a dynamical system into 2 categories:

– conservative (linearized, undamped)

– dissipative (linearized, damped)

depending on whether the phase volumes *stay constant* or *contract*, respectively

$$\frac{d^2 \theta}{d t^2} + \frac{d \theta}{d t} + \theta = 0 \rightarrow \omega = \theta = 0$$

Attractor: Point in phase space: a finite set of initial coordinates (θ, ω) converges to it. The set of curves that divide one basin of attraction from another is called **separatrix**.

8.2.2 Poincaré Section

Fully nonlinear, driven, and damped oscillation. For moderately driven pendulum system, the resulting closed orbit is an attractor, it is called a **limit cycle**.

A Poincaré section is constructed by viewing the phase space diagram *stroboscopically* in such a way that the motion is observed periodically. For a driven pendulum, the strobe period is the period of the forcing ω_D .

8.3 Visualization of the Pendulum's Dynamics

$$\frac{d \omega}{d t} = -\frac{\omega}{q} - \sin \theta + g \cos \phi$$

$$\frac{d \theta}{d t} = \omega$$

$$\frac{d \phi}{d t} = \omega_D$$

8.3.1 Sensitivity to Initial Conditions

Observe the phase space evolution of a block of pendulum states.

8.3.2 Phase Diagrams: Chaos and Self-Similarity

– Drive force amplitudes g will be varied.

– $\omega_D = \frac{2}{3}, q = 2$

3-D space (θ, ω, ϕ) , 2-D space, Poincaré sections

$g = 1.5$: Poincaré section shows a chaotic attractor, called **strange attractor**. The fine structure, when magnified, resembles the gross structure. This property is called **self-similarity**. One can characterize these objects by non-integer **fractal dimension**:

$d > 1$ but $d < 2$, the attractor is more space-filling than a line but less than an area.

8.3.3 Bifurcation Diagrams

View the dynamics more globally over a range of parameter values: **bifurcation diagrams**. In

dynamics, a change in the number of solutions to a differential equation if a parameter is varied is called bifurcation.

Pendulum: examine a graph of ω at a fixed phase in the drive cycle versus the drive amplitude.

Whenever another stable stationary solution pops up, one has the effect of **period doubling**. System cycles between two values of ω for each set of initial conditions.

Mechanical oscillator possesses 2 stable oscillation frequencies; the system can be tuned to either of them by appropriate initial conditions: *mechanical flip-flop*.

8.4 Towards an Understanding of Chaos

$$x_{n+1} = f(\mu, x_n)$$

x_n n-th value of $x \in (0, 1)$; μ : parameter; $f: (0, 1) \rightarrow (0, 1)$ map

8.4.1 The Logistic Map

$$x_{n+1} = f(x_n) = \mu x_n (1 - x_n), x \in [0, 1]$$

$$\frac{dx}{dt} = \mu x (1 - x) \quad \text{Verhulst, 1845}$$

The fixed point is stable for all initial conditions when $\mu = 2$. Remains true for all μ where $|f'(x)| < 1$ at the intersection of f and $x_{n+1} = x_n$. As soon as $|f'(x)| > 1$ at the intersection, the fixed point oscillates. The passage to chaos through a sequence of period doublings is one important feature of the logistic map. The period doubling mechanism is one **route to chaos**.

The ratio of spacings between consecutive values of μ at the bifurcations approaches an universal constant, called **Feigenbaum number**.

$$\lim_{k \rightarrow \infty} \frac{\mu_k - \mu_{k-1}}{\mu_{k+1} - \mu_k} = \delta = 4.669201 \dots$$

8.4.2 Lyapunov Exponent

= Quantitative measure of the sensitive dependence upon initial conditions.

Initial states, x and $x + \varepsilon$, then after n iterations their divergence may be characterized by

$$\varepsilon(n) \approx \varepsilon e^{\lambda n}$$

where Lyapunov exponent λ gives the *average rate of divergence*.

If $\lambda < 0 \Rightarrow$ evolution is not chaotic.

If $\lambda > 0 \Rightarrow$ nearby trajectories diverge \Rightarrow chaotic.

$$x_{n+1} = f(x_n)$$

After n-th step:

$$f^{(n)}(x_0 + \varepsilon) - f^{(n)}(x_0) \approx \varepsilon e^{n\lambda} \text{ or}$$

$$\ln \left[\frac{f^{(n)}(x_0 + \varepsilon) - f^{(n)}(x_0)}{\varepsilon} \right] \approx n\lambda$$

$f^{(n)}(x) = f(f(f(\dots f(x))))$ is the value after n-th iteration. For small ε ,

$$\lambda(x_0) = \lim_{n \rightarrow \infty} \frac{1}{n} \ln \left| \frac{df^{(n)}(x_0)}{dx_0} \right|$$

Apply chain rule for these second iteration:

$$\left. \frac{d}{dx} f^{(2)}(x) \right|_{x_0} = \left. \frac{d}{dx} f(f(x)) \right|_{x_0} = f'(f(x_0)) \cdot f'(x_0) = f'(x_1) \cdot f'(x_0)$$

$$x_1 = f(x_0)$$

$$\lambda(x_0) = \lim_{n \rightarrow \infty} \frac{1}{n} \ln \left| \frac{d f^{(n)}(x_n)}{d x_0} \right| = \lim_{n \rightarrow \infty} \frac{1}{n} \ln \left| \prod_{i=0}^{n-1} f'(x_i) \right| = \lim_{n \rightarrow \infty} \frac{1}{n} \sum_{i=0}^{n-1} \ln |f'(x_i)|$$

The Lyapunov exponent gives the stretching rate per iteration, averaged over the trajectory.

8.4.3 Intermittency Route to Chaos

By **intermittency** we mean the occurrence of a signal that alternates randomly between long, regular, periodic phases (so-called **intermissions**) and relatively short irregular bursts.

$x_{n+1} = f(x_n)$ if map approaches but does not cross the line $x_{n+1} = x_n$ and runs nearly tangential, one gets intermittency:

Celestial mechanics: Asteroids between Mars and Jupiter: maintain seemingly stable, almost circular orbits for years, suddenly develop large eccentricities \Rightarrow shooting stars.

8.4.4 Phase Locking

Phase locking is said to occur when the ratio of the frequency of a pendulum to that of the forcing becomes locked to a ratio n/m ($n, m \in \mathbb{N}$), over some finite domain of parameter values.

Standard Map

$$\Theta_{n+1} = \left[\Theta_n + \Omega - \frac{K}{2\pi} \sin(2\pi \Theta_n) \right] \text{mod } 1$$

There are 2 parameters (Ω, K) and $\Theta_n \in (0, 1)$. The modulo function guarantees periodic boundary conditions. Ω is rotation frequency of „winding number“ in the absence of nonlinearity ($K = 0$). K strength of nonlinear coupling of the oscillator to the forcing.

$K = 0$:

$$\Theta_{n+1} = \Theta_n + \Omega \text{ mod } 1;$$

$\Omega = 0.4$:	0.3	0.7	0.1	0.5	0.9	0.3
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After 5 iterations return to initial value; 2 revolutions; $\Rightarrow W = 2/5 = 0.4 = \Omega$.

Whenever Ω is rational, the map is periodic. When nonlinear term is added, mode locking occurs: the motion becomes periodic even when Ω is irrational.

8.5 Characterization of Chaotic Attractors: Fractals

Dimension of a geometrical object: **Hausdorff-dimension** or **capacity-dimension**.

Consider a curve of total length L . Assume that we can completely cover this line by $N(\varepsilon)$ one-dimensional boxes of size ε on a side.

$$N(\varepsilon) \cdot \varepsilon = L ; N(\varepsilon) = L \frac{1}{\varepsilon} ;$$

2-D square of side L can be covered by

$$N(\varepsilon) = L^2 \left(\frac{1}{\varepsilon} \right)^2$$

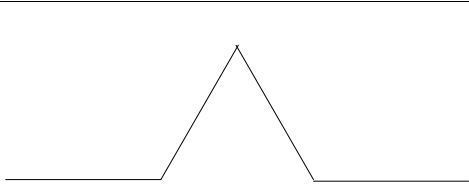
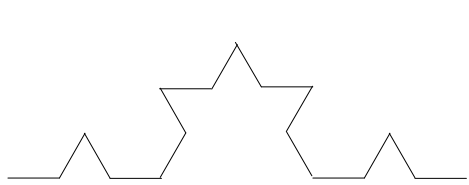
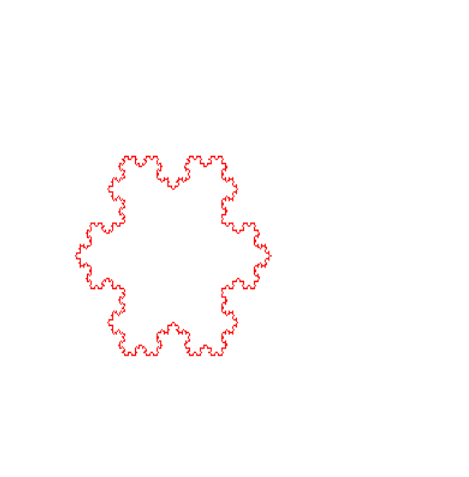
boxes.

For 3-D cube: Exponents are 3.

$$N(\varepsilon) = L^d \left(\frac{1}{\varepsilon} \right)^d \Rightarrow d = \frac{\ln N(\varepsilon)}{\ln L + \ln(1/\varepsilon)}$$

$$d_{\text{Hausdorff}} = \lim_{\varepsilon \rightarrow 0} \frac{\ln N(\varepsilon)}{\ln(1/\varepsilon)}$$

Koch curve:

	N	ε
	1	1
	4	1/3
	16	1/9
	4^n	$\left(\frac{1}{3} \right)^n$

$$d_H = \frac{n \ln 4}{n \ln 3} = \frac{\ln 4}{\ln 3} = 1.26$$

9. Basic Concepts of Electrodynamics

9.1 Electrostatics

Static charge distribution $\rho(\vec{r})$. Force that is felt by a test charge ($+e$) due to $\rho(\vec{r})$:

$$\text{Force } \vec{F} = e \vec{E}(\vec{x})$$

$$\vec{E}(\vec{x}) = \frac{1}{4\pi\epsilon_0} \int \rho(\vec{x}') \frac{(\vec{x} - \vec{x}')}{|\vec{x} - \vec{x}'|^3} d^3x'$$

ϵ_0 = vacuum permittivity or dielectric constant of vacuum

$$\epsilon_0 \vec{\nabla} \cdot \vec{E} = \rho$$

Gauss's Law

$$\vec{E}(\vec{x}) = -\frac{1}{4\pi\epsilon_0} \vec{\nabla} \int \frac{\rho(\vec{x}')}{|\vec{x} - \vec{x}'|} d^3x' \equiv -\vec{\nabla} \phi(\vec{x})$$

curl grad $\equiv 0$:

$$\vec{\nabla} \times \vec{E} = 0$$

$$\nabla^2 \phi = -\frac{\rho}{\epsilon_0}$$

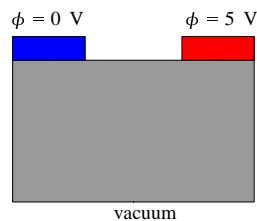
Poisson equation

PDE for $\phi(\vec{x})$:

(a) ρ

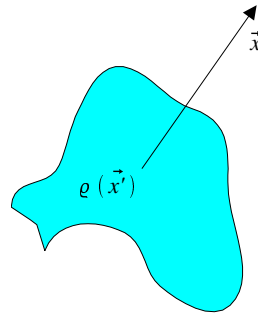
(b) boundary conditions for $\phi(\vec{x})$ on a closed surface
2 types of boundary conditions that occur frequently:

- Dirichlet boundary condition: $\phi = \text{preset value}$



- von-Neumann boundary condition: $E_n = -\vec{\nabla}_n \phi$ (= normal derivative of ϕ) is specified on a closed surface: $\vec{\nabla}_n \phi = 0$

9.1.1 Multipole Expansion



$$\phi(\vec{x}) = \frac{1}{4\pi\epsilon_0} \int \frac{\rho(\vec{x}')}{|\vec{x} - \vec{x}'|} d^3x'$$

Taylor expansion of $1/|\vec{x} - \vec{x}'|$ in terms of powers of \vec{x}' :

$$\left. \frac{\partial}{\partial x'_i} \frac{1}{|\vec{x} - \vec{x}'|} \right|_{\vec{x}'=0} = - \left. \frac{\partial}{\partial x_i} \frac{1}{|\vec{x} - \vec{x}'|} \right|_{\vec{x}'=0} = - \frac{\partial}{\partial x_i} \frac{1}{r}; \quad r \equiv |\vec{x}|;$$

$$\frac{1}{|\vec{x} - \vec{x}'|} = \frac{1}{r} - \sum_{i=1}^3 x'_i \frac{\partial}{\partial x_i} \frac{1}{r}$$

$$f(\vec{x} - \vec{x}') = f(\vec{x}) + \sum_{i=1}^3 x'_i \frac{\partial f}{\partial x'_i} + \dots + \frac{1}{2} \sum_{i,j=1}^3 x'_i x'_j \frac{\partial}{\partial x_i} \frac{\partial}{\partial x_j} \frac{1}{r} + \dots$$

$$4\pi\epsilon_0 \phi(\vec{x}) = \frac{q}{r} + \frac{\vec{p} \cdot \vec{x}}{r^3} + \frac{1}{2} \sum_{i,j=1}^3 Q_{ij} \frac{x_i x_j}{r^5} + \dots$$

$q = \int d^3x' \rho(\vec{x}')$ is total charge

$\vec{p} = \int d^3x' \vec{x}' \rho(\vec{x}')$ dipole moment

$Q_{ij} = \int d^3x' (3x'_i x'_j - r'^2 \delta_{ij}) \rho(\vec{x}')$ quadrupole moment

$$\Delta \frac{1}{r} = 0 \text{ for } r \neq 0$$

9.2 Magnetostatics

$\vec{\nabla} \cdot \vec{B} = 0$ no free magnetic charges, no monopoles

Electric current density: \vec{J} = in unit of positive charge crossing unit area per unit time.

Direction of motion $\parallel \vec{J}$

Units: Amperes per square meter

Current density is confined to a wire \Rightarrow current = $J \cdot A$.

Microscopically: point charges at \vec{x}_i with velocities \vec{v}_i :

$$\rho(\vec{x}, t) = \sum_i q_i \delta(\vec{x} - \vec{x}_i(t))$$

$$\vec{J}(\vec{x}, t) = \sum_i q_i \vec{v}_i(t) \delta(\vec{x} - \vec{x}_i(t))$$

δ : Dirac's delta function (is a functional):

$$\int d^3x f(x) \delta(x - x_0) = f(x_0)$$

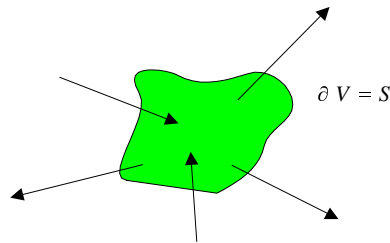
Distribution:

$$\lim_{\varepsilon \rightarrow 0} \int d^3 x f(x) \frac{\varepsilon}{(x - x_0)^2 + \varepsilon^2} = f(x_0)$$

Conservation of charge demands relation between $\rho \leftrightarrow \vec{J}$ via continuity equation

$$\vec{J}(\vec{x}, t) \Delta V = \int_{\Delta V} d^3 x \rho(\vec{x}) \vec{v}(\vec{x}, t)$$

$$\frac{d}{dt} \int_V d^3 x' \rho(\vec{x}', t) + \oint_S d\vec{S} \cdot \vec{J}(\vec{x}', t) = 0$$



Gauss's theorem:

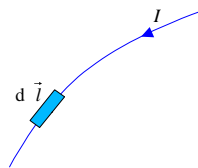
$$\int_V d^3 x' \left(\frac{\partial \rho(\vec{x}', t)}{\partial t} + \text{div} \vec{J}(\vec{x}', t) \right) = 0$$

$$\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot \vec{J} = 0$$

Magnetostatics: steady-state phenomena $\Rightarrow \vec{\nabla} \cdot \vec{J} = 0$

Consider a filamentary wire which carries a constant current I . In the presence of other conductors (e.g. current-carrying wires) that wire feels a force. The elemental force $d\vec{F}$ experienced by a current element $d\vec{l}$ of the wire obeys

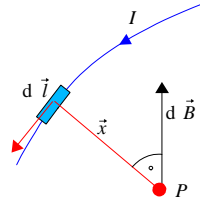
$$dF \propto I, dF \propto |d\vec{l}|, d\vec{F} \perp d\vec{l}$$



$$d\vec{F}(\vec{x}) = I d\vec{l} \times \vec{B}(\vec{x})$$

magnetic induction \vec{B} or **magnetic flux density** \vec{B}

We now determine the magnitude of \vec{B} generated by a current-carrying wire: Consider again a filamentary wire.



The elemental flux density $d\vec{B}$ generated by a current element $d\vec{l}$ at an observation point P is

$$d\vec{B} = \frac{\mu_0}{4\pi} I \frac{d\vec{l} \times \vec{x}}{|\vec{x}|^3}$$

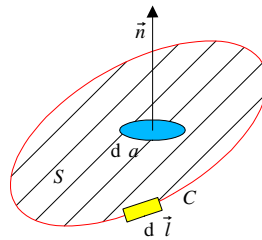
$\mu_0 = (\epsilon_0 c^2)^{-1}$ vacuum permeability

Biot-Savart-Law

$$\vec{B}(\vec{x}) = \frac{\mu_0}{4\pi} \int \vec{J}(\vec{x}') \times \frac{(\vec{x} - \vec{x}')}{|\vec{x} - \vec{x}'|^3} d^3 x' = \frac{\mu_0}{4\pi} \vec{\nabla} \times \int \frac{\vec{J}(\vec{x}')}{|\vec{x} - \vec{x}'|} d^3 x'$$

$$\Rightarrow \vec{\nabla} \cdot \vec{B} = 0 \quad (\text{corresponding to } \vec{\nabla} \times \vec{E} = 0)$$

$$\vec{\nabla} \times \vec{B}(\vec{x}) = \mu_0 \vec{J}(\vec{x})$$



$$\int_S \vec{\nabla} \times \vec{B} \cdot \vec{n} d a = \mu_0 \int_S \vec{J} \cdot \vec{n} d a$$

$$\oint_C \vec{B} \cdot d\vec{l} = \mu_0 \int_S \vec{J} \cdot \vec{n} d a = \mu_0 I$$

I is the total current passing through the closed curve C . Ampere's law.

$$\vec{B}(\vec{x}) = \vec{\nabla} \times \vec{A}(\vec{x})$$

$$\vec{A}(\vec{x}) = \frac{\mu_0}{4\pi} \int \frac{\vec{J}(\vec{x}')}{|\vec{x} - \vec{x}'|} d^3 x' + \nabla \psi(\vec{x})$$

$\vec{A} \rightarrow \vec{A} + \nabla \psi$ **Gauge transformation**

$$\vec{\nabla} \times (\vec{\nabla} \times \vec{A}) = \mu_0 \vec{J}$$

$$\vec{\nabla} (\vec{\nabla} \cdot \vec{A}) - \nabla^2 \vec{A} = \mu_0 \vec{J}$$

$$\vec{\nabla} \cdot \vec{A} = 0; \quad (\text{but } \vec{\nabla} \cdot \nabla \psi \neq 0 \text{ for arbitrary } \psi)$$

\Rightarrow **Coulomb gauge** (fixes ψ)

$$\nabla^2 \vec{A}(\vec{x}) = -\mu_0 \vec{J}$$

Magnetic field \vec{H} : $\vec{B} = \mu_0 \vec{H}$

$$\Rightarrow \text{Ampere's law: } \vec{\nabla} \times \vec{H} = \vec{J}$$

$$\text{Dielectric displacement: } \vec{D} = \epsilon_0 \vec{E}$$

$$\Rightarrow \vec{\nabla} \cdot \vec{D} = \rho \quad (\text{div } \vec{D} = \rho)$$

Force always contains \vec{E} and \vec{B} (H and D are only auxiliary elements)

9.3 Time-Varying Field

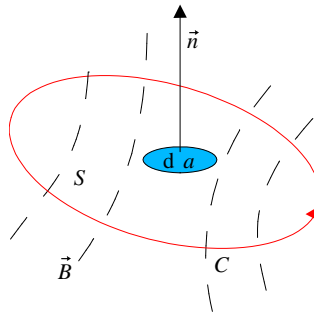
Time-dependent magnetic fields induce electric fields and vice versa \Rightarrow **electromagnetic fields**

9.3.1 Faraday's Law

Faraday 1831 observed that a transient current is induced in a circuit if

- the steady current flowing in an adjacent circuit is turned on or off
- the adjacent circuit with a steady current flowing is moved relative to the first circuit
- a permanent magnet is thrust into or out of the circuit

Faraday interpreted (correctly) the transient current flow as being due to a changing magnetic flux linked by the circuit. The changing flux induces an electric field around the circuit, the line integral of which is called **electromotive force** \tilde{E} :



The **magnetic flux** passing through the circuit is

$$F = \int_S \vec{B} \cdot \vec{n} \, d a$$

The **electromotive force** around the circuit is

$$\tilde{E} = \oint_C \vec{E}' \cdot d \vec{l}$$

\vec{E}' is the electric field at the element $d \vec{l}$ of the circuit measured in the rest frame of the circuit.

$$\text{Faraday: } \tilde{E} = - \frac{d F}{d t}$$

The **induced electromotive force** around the circuit is proportional to the time rate of change of magnetic flux linking the circuit.

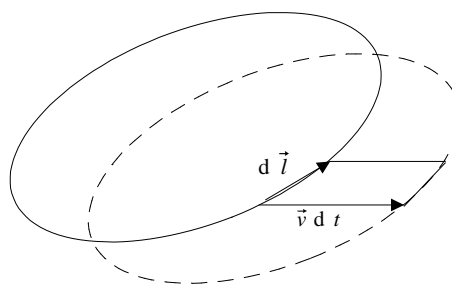
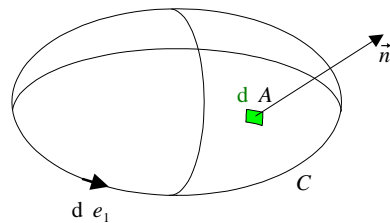
The sign is specified by **Lenz's law**: induced current (and accompanying magnetic flux) is in such a direction as to oppose the change of flux through the circuit.

Experimentally verified that the same current is induced in a circuit whether it is moved while the circuit through which current is flowing is stationary or it is held fixed while the current-carrying

circuit is moved in the same relative manner.

We can write Faraday's law more generally as

$$\oint_C \vec{E}' \cdot d\vec{l} = -\frac{d}{dt} \int_S \underbrace{\vec{B} \cdot \vec{n}}_{d\vec{a}} da$$



Let us move the circuit C with velocity \vec{v} .

The area of the circuit changes by $d\vec{a} = \vec{v} dt \times d\vec{l}$; $d\vec{a} = \vec{n} da$.

$$\frac{d}{dt} \int_S \vec{B} \cdot \vec{n} da = \int_S \frac{\partial \vec{B}}{\partial t} \cdot \vec{n} da + \int_S \vec{B} \cdot \frac{\partial \vec{a}}{\partial t} = \int_S \frac{\partial \vec{B}}{\partial t} \cdot \vec{n} da + \oint_C \underbrace{\vec{B} \cdot (\vec{v} \times d\vec{l})}_{= d\vec{l} \cdot (\vec{B} \times \vec{v})}$$

$$\oint_C [\vec{E}' - \vec{v} \times \vec{B}] \cdot d\vec{l} = -\int_S \frac{\partial \vec{B}}{\partial t} \cdot \vec{n} da$$

In an inertial frame: Let us consider S and C fixed in space.

$$\oint_C \vec{E} \cdot d\vec{l} = -\int_S \frac{\partial \vec{B}}{\partial t} \cdot \vec{n} da$$

\vec{E} is electric field in inertial system. Galilean invariance implies $\Rightarrow \vec{E}'$ in the moving system,

$$\vec{E}'_{BS} = \vec{E}_{IS} + \vec{v} \times \vec{B}$$

Faraday's law in differential form: \vec{E}, \vec{B} are defined in same frame.

$$\int_S \left(\vec{\nabla} \times \vec{E} + \frac{\partial \vec{B}}{\partial t} \right) \cdot \vec{n} da = 0$$

$$\vec{\nabla} \times \vec{E} + \frac{\partial \vec{B}}{\partial t} = 0$$

9.3.2 Maxwell's Displacement Current and Maxwell's Equations

Ampere's law: $\vec{\nabla} \times \vec{H} = \vec{J}$, for steady state $\vec{\nabla} \cdot \vec{J} = 0$.

$$\vec{\nabla} \cdot \vec{J} = \vec{\nabla} \cdot (\vec{\nabla} \times \vec{H}) = 0;$$

$$\vec{\nabla} \cdot \vec{J} + \frac{\partial \rho}{\partial t} = 0$$

Coulomb's law: $\vec{\nabla} \cdot \vec{D} = \rho$ or $\epsilon_0 \vec{\nabla} \cdot \vec{E} = \rho$

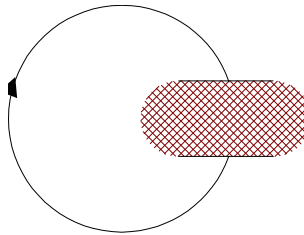
$$\vec{\nabla} \cdot \vec{J} + \frac{\partial \rho}{\partial t} = \vec{\nabla} \cdot \left(\vec{J} + \frac{\partial \vec{D}}{\partial t} \right) = 0$$

Maxwell 1865:

$$\vec{J} \rightarrow \vec{J} + \frac{\partial \vec{D}}{\partial t}$$

Ampere's law:

$$\vec{\nabla} \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$$



⇒ Electromagnetic radiation!

Light is an electromagnetic wave phenomenon and these waves of all frequencies can be produced.

$$\begin{aligned} \vec{\nabla} \cdot \vec{D} &= \rho \text{ (Gauss's law)} \\ \vec{\nabla} \times \vec{H} - \frac{\partial \vec{D}}{\partial t} &= \vec{J} \text{ (Ampere's law)} \\ \vec{\nabla} \cdot \vec{B} &= 0 \text{ (no magnetic monopoles)} \\ \vec{\nabla} \times \vec{E} + \frac{\partial \vec{B}}{\partial t} &= 0 \text{ (Faraday+Lenz)} \end{aligned}$$

9.4 Wave Propagation: Plane Electromagnetic Waves

No source, infinite space

$$\vec{\nabla} \cdot \vec{E} = 0$$

$$\frac{1}{\mu_0} \vec{\nabla} \times \vec{B} - \epsilon_0 \frac{\partial \vec{E}}{\partial t} = 0 \quad / \quad \vec{\nabla} \times$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{E} + \frac{\partial \vec{B}}{\partial t} = 0 \quad / \quad \vec{\nabla} \times$$

$$\underbrace{\vec{\nabla} \times (\vec{\nabla} \times \vec{B})}_{\vec{\nabla}(\vec{\nabla} \cdot \vec{B}) - \nabla^2 \vec{B}} - \frac{1}{c^2} \frac{\partial}{\partial t} (\vec{\nabla} \times \vec{E}) = 0$$

$$-\nabla^2 \vec{B} + \frac{1}{c^2} \frac{\partial^2}{\partial t^2} \vec{B} = 0$$

$$\Rightarrow \nabla^2 u - \frac{1}{c^2} \frac{\partial^2 u}{\partial t^2} = 0 \quad u = E_i, B_i$$

$$u = e^{i \vec{k} \cdot \vec{x} - i \omega t}$$

Wavevector \vec{k} and frequency ω

$$-k^2 + \frac{\omega^2}{c^2} = 0$$

$$k = \frac{\omega}{c} = \frac{2\pi}{\lambda}$$

If we consider waves propagating in the x -direction, fundamental solution:

$$u(x, t) = A e^{i k x - i \omega t} + B e^{-i k x - i \omega t} = A e^{i k (x - c t)} + B e^{-i k (x + c t)}$$

The general solution of the wave equation is

$$u(x, t) = f(x - v t) + g(x + v t)$$

\Rightarrow The equation represents traveling waves; traveling to the right and the left with velocities of propagation $v = c$.

$v = \omega/k$ is called the **phase velocity** of the wave. The **wavelength** is $\lambda = (2\pi)/k$.

Convention: Physical electric and magnetic fields by taking real parts of complex quantities, plane wave fields are

$$\vec{E}(\vec{x}, t) = \vec{\varepsilon}_1 E_0 e^{i \vec{k} \cdot \vec{x} - i \omega t}$$

$$\vec{B}(\vec{x}, t) = \vec{\varepsilon}_2 B_0 e^{i \vec{k} \cdot \vec{x} - i \omega t}$$

E_0 and B_0 are complex amplitudes which are constant in space and time.

$\vec{\varepsilon}_1, \vec{\varepsilon}_2$ are constant real unit vectors.

$$\vec{\nabla} \cdot \vec{E} = 0 \Rightarrow \vec{\varepsilon}_1 \cdot \vec{k} = 0$$

$$\vec{\nabla} \cdot \vec{B} = 0 \Rightarrow \vec{\varepsilon}_2 \cdot \vec{k} = 0$$

Direction of propagation is $\vec{k} \Rightarrow$ **transverse waves!**

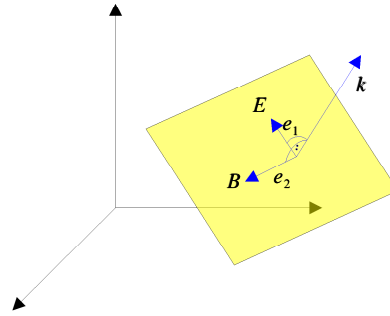
$$\vec{\nabla} \times \vec{E} + \dot{\vec{B}} = 0 \Rightarrow i \left[(\vec{k} \times \vec{\varepsilon}_1) E_0 - \omega \vec{\varepsilon}_2 B_0 \right] e^{i \vec{k} \cdot \vec{x} - i \omega t} = 0$$

\Rightarrow solution:

$$\vec{\varepsilon}_2 = \frac{\vec{k} \times \vec{\varepsilon}_1}{k}$$

$$B_0 = \frac{1}{c} E_0$$

$(\vec{\varepsilon}_1, \vec{\varepsilon}_2, \vec{k})$ form a set of orthogonal vectors and \vec{E}, \vec{B} are in phase and possess a constant ratio.



⇒ Waves in vacuum (no sources) are transverse waves propagating in the direction of \vec{k} . Since $\vec{E} \parallel$ fixed direction $\vec{\epsilon}_1$, we call such a wave **linearly polarized** with polarization vector $\vec{\epsilon}_1$.

9.4.1 Superposition of Waves

Since ME are *linear* PDEs, any superposition of plane wave solutions is a solution as well. Waves in x-direction:

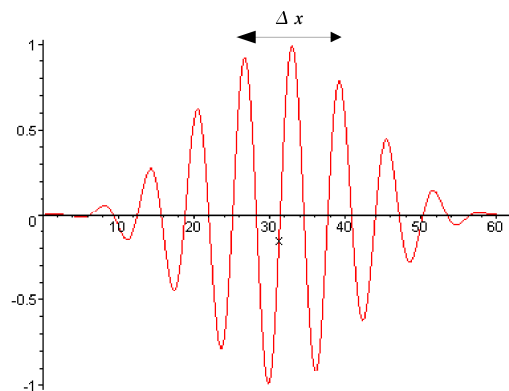
$$u(x, t) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} A(k) e^{ikx - i\omega t} dk$$

The amplitude $A(k)$ describes the properties of the linear superposition of the different waves. From Fourier analysis,

$$A(k) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} u(x, 0) e^{-ikx} dx$$

$$f(x) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} A(k) e^{ikx} dk, \quad A(k) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} e^{-ikx} f(x) dx$$

$$\frac{1}{2\pi} \int_{-\infty}^{\infty} e^{i(k-k')x} dx = \delta(k - k'), \quad \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{ik(x-x')} dk = \delta(x - x')$$



$$\Delta x \cdot \Delta k \geq \frac{1}{2}$$

In vacuum, a pulse or wave packet propagates in such a way that the packet does not change its shape. In a medium, however,

$$\omega(k) = \frac{ck}{n(k)},$$

so that

$$v = \frac{\omega}{k} = \frac{c}{n(k)}$$

depends on k or on the wavelength $\lambda = (2\pi)/k$. Then, wave packet will spread with time as it travels along, because the waves of different wavelength propagate at different speeds. This phenomenon is called **dispersion**.